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FORTRAN IV PROGRAMS FOR THE EXTRACTION OF POTENTIAL WELL PARAMETERS FROM
THE ENERGY DEPENDENCE OF TOTAL ELASTIC SCATTERING CROSS SECTIONS

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TECHNICAL NOTES

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FORTRAN IV PROGRAMS FOR THE EXTRACTION OF POTENTIAL WELL PARAMETERS FROM
THE ENERGY DEPENDENCE OF TOTAL ELASTIC SCATTERING CROSS SECTIONS*

by

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<u>SECTION</u>	<u>SUBSECTION</u>	<u>PAGE</u>	<u>LINE</u>	<u>REMARK</u>
I		3	4	$2\pi/3 \beta = 2\pi\beta/3$
IV	PHASHT	PL*	2	obscured is C(5)
			3	obscured is - 0.0544
VI	FINAL	PL*	11	obscured is R
VI	SYMQR	PL*	139	Replace 1.D-21 with 1.D-16 *ENORM/(N*N)
			145	Replace 1.D-21 with 1.D-16 *ENORM/(N*N)
VII	JWKB	2		Pages 2 and 3 are facing incorrectly
		3		

* PL = Program Listing

PREFACE

An attempt has been made to keep the programs as subroutine oriented as possible. Usually only the main programs are directly concerned with the problem of total cross sections. In particular the subroutines POLFIT (IV.A), BILINR (V.B), GASS59/MAXLIK (VI.D), SYMQR (VI.E), MATIN (VI.F), STUDNT (VI.G), DNTERP (VII.E), DIFTAB (VII.F), FORDIF (VII.G), EPSALG (VII.H), REGFAL (VII.I), AND ADSIMP (VII.J), are completely general, and are concerned only with the problems of numerical analysis and statistics. Each subroutine is independently documented.

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I. DISCUSSION*

The total cross section $Q(v)$, where v is the relative velocity, is assumed to be a sum of two components: $Q_{SLL}(v)$, dependent upon the long-range force constant C_6 , and $\Delta Q_g(v)$, an oscillatory term due to the presence of glory extrema

$$Q(v) = Q_{SLL}(v) + \Delta Q_g(v) \quad (I-1)$$

where

$$Q_{SLL}(v) \simeq 8.083 \left(\frac{C_6}{\hbar v} \right)^{2/5} \quad (I-2a)$$

$$\Delta Q_g(v) \simeq \frac{4\pi^{3/2}}{k^2} \frac{L_g}{(-\eta_m'')^{1/2}} \sin(2\eta_m - \frac{3\pi}{4}) \quad (I-2b)$$

where $k = \mu v / \hbar$ is the wavenumber, L_g is value of the orbital quantum number l corresponding to η_m , a maximum in the phase shift, and η_m'' is the second-derivative of η_m with respect to l evaluated at L_g .

It can be shown that by expanding about the high-velocity limit, (2b) may be written

$$\Delta Q_g(v) = (2\pi r_m)^{3/2} g_0 \left(\frac{\hbar v}{\epsilon} \right)^{1/2} \left[1 + \frac{H_1 \epsilon}{E} + \frac{H_2 \epsilon^2}{E^2} + \dots \right] \sin \phi \quad (I-3)$$

where $E = \frac{1}{2} \mu v^2$ is the energy,

$$\phi = -\frac{3\pi}{4} + \frac{4\epsilon r_m}{\hbar v} \left(a_1 + \frac{A_1 \epsilon}{E} + \frac{A_2 \epsilon^2}{E^2} + \dots \right) \quad (I-4)$$

* For a more complete description of the derivations of the formulae see
Wisc. Theor. Chem. Institute Report WIS-TCI-469 (1972).

and r_m is the position of the minimum of (of depth ϵ) the potential. The constants g_0, a_1 are related to the curvature of the potential well at $r = r_m$, and the constants $H_1, H_2, \dots, A_1, A_2, \dots$, were found to be to a good approximation independent of the curvature, ϵ , and r_m , and of the form of the potential. Furthermore, for the energy range $1 \leq E^* \leq 100$, where $E^* = E/\epsilon$ is the reduced energy, it was found only the terms H_1 and A_1, A_2, A_3 and A_4 were required. For a Lennard-Jones 12-6 potential, i.e.,

$$V(r) = \epsilon \left[\left(\frac{r_m}{r} \right)^{12} - 2 \left(\frac{r_m}{r} \right)^6 \right]$$

the values of the constants are:

$$g_0 = 0.186299 \quad (I-5a)$$

$$H_1 = 3.267 \pm 0.80 \quad (I-5b)$$

$$a_1 = 0.4215587 \quad (I-5c)$$

$$A_1 = -0.1655 \pm .0016 \quad (I-5d)$$

$$A_2 = 0.1057 \pm 0.0160 \quad (I-5e)$$

$$A_3 = -0.0544 \pm 0.0160 \quad (I-5f)$$

$$A_4 = 0.0139 \pm 0.0084 \quad (I-5g)$$

In terms of free parameters, (1) may be rewritten

$$Q(v) = \gamma_1 v^{-2/5} + \gamma_2 v^{1/2} \left(1 + \frac{H_1 \epsilon}{E} \right) \sin \phi \quad (I-6)$$

and

$$\phi = -\frac{3\pi}{4} + \frac{\gamma_3}{v} + \frac{\gamma_4}{vE} \left(A_1 + \frac{A_2 \epsilon}{E} + \frac{A_3 \epsilon^2}{E^2} + \frac{A_4 \epsilon^3}{E^3} \right) \quad (I-7)$$

where

$$\begin{aligned}\gamma_1 &= 8.083 \left(\frac{C_6}{\hbar} \right)^{2/5} \\ \gamma_2 &= (2\pi r_m)^{3/2} g_0 (\hbar/\epsilon)^{1/2} \\ \gamma_3 &= 4a_1 \epsilon r_m / \hbar \\ \gamma_4 &= 4\epsilon^2 r_m / \hbar\end{aligned}$$

(I-8)

It has been shown previously that when the r^{-8} term in the potential begins to affect the cross section, it may be accounted for by replacing $Q_{\text{SLL}}(v)$ in (1) by $Q_{\text{SLL}}(v) + 2\pi/3 \beta$, where $\beta = C_8/C_6$.

It is clear from the form of (I-6) that $Q(v)$ has an oscillatory component. The condition for extrema in Q is that $\sin \phi = \pm 1$, which can be shown to lead to:

$$\left(N - \frac{3}{8}\right) v_g = \frac{2\epsilon r_m}{\hbar} \left(a_1 + \frac{A_1 \epsilon}{E} + \frac{A_2 \epsilon^2}{E^2} + \frac{A_3 \epsilon^3}{E^3} + \frac{A_4 \epsilon^4}{E^4}\right) \quad (\text{I-9})$$

where the maxima and minima in $Q(v)$ are indexed by $N(v_g)$ in the order they occur, i.e., $N = 1$ corresponds to the first maximum, $N = 1.5$ corresponds to the first minimum, $N = 2$ is the second maximum, etc. The quantities v_g are the associated values of v at the extrema.

II. UNITS

All of the results and programs below assume the following system of units:

$$\text{Mass} \quad M = 10^{-24} \text{ g} = 1 \text{ ppg (picopicogram)}$$

$$\text{Length} \quad L = 10^{-8} \text{ cm} = 1 \text{ \AA}^{\circ} (\text{Angstrom})$$

$$\text{Time} \quad T = 10^{-13} \text{ sec} = 1 \text{ dps (decipicosecond)}$$

In this sytem,

$$1 \text{ amu} = 1.660531 \text{ ppg}$$

$$1 \text{ a.u.} = 0.52917715 \text{ \AA}$$

$$1 \text{ Km/sec} = 1 \text{ \AA}^{\circ}/\text{dps}$$

$$1 \text{ eV} = 160.21917 \text{ cpe}$$

$$1 \text{ Kcal/mole} = 6.94793 \text{ cpe}$$

$$h = 6.626196 \text{ cpe-dps}$$

$$\hbar = 1.0545919 \text{ cpe-dps}$$

$$kT = 1.380622 \text{ cpe} @ T = 100^{\circ}\text{K}$$

III. XSECT

The purpose of the main program XSECT is to calculate total cross sections $Q(v)$ by means of (I-6)-(I-8). The assumption is made that H_1 and A_1, A_2, A_3, A_4 are those for the L-J(12-6) potential given in (I-5).

The first card of the data set contains (18A4) 72 columns of title information, which is reproduced at the top of the output.

The second card of the data specifies N, MU, EPS, A1, B0, C1, C6, in that order, according to the format (I5, 6F10.4, E15.6), where:

N - No. of velocities for which $Q(v)$ is to be calculated

MU - μ (reduced mass)

EPS - ϵ

RM - r_m

A1 - a_1 (I-5c)

B0, C1 - b_0 and c_1 are related to the leading terms in the expansion in powers of $1/E^*$ of L_g and η_m'' respectively.

Since the only quantity required is $g_0 = b_0/c_1^{1/2}$, b_0 may be set equal to g_0 and c_1 to 1.

C6 = C_6 the long-range force constant.

The succeeding cards of the data contain the velocities $V(I)$, $I = 1, \dots, N$, for which the $Q(v)$ are to be calculated, according to the format (8F10.4).

The output of the program is a table of the values of $V(I)$, QSL, DELQ, Q, and QF for $I = 1, \dots, N$, where

$$Q_{SLL} = Q_{SLL}(v)$$

$$\Delta Q_g = \Delta Q_g(v)$$

$$Q = Q(v) = Q_{SLL}(v) + \Delta Q_g(v)$$

$$QF = \Delta Q_g(v) / Q_{SLL}(v)$$

XSECT

D COMPILED BY FOR-V S7E6 ON 06 SEP 71 AT 17:41:11.

GE USED: CODE(1) 000270; DATA(0) 000515

```
1* C      PROGRAM TO GENERATE RAPID CROSS SECTIONS
2*      REAL MU
3*      DIMENSION V(200),A(4),TITLE(18)
4*      DATA A/-0.1655,0.1057,-0.0544,0.0139/,H1/3.267/
5*      DATA PI/3.14159265/,HCROSS/1.0545919/
6*      100 READ (5,5) (TITLE(I),I=1,18)
7*      5   FORMAT (18A4)
8*      WRITE (6,6) (TITLE(I),I=1,18)
9*      6   FORMAT (1H1,10X,18A4)
10*     READ (5,10) N,MU,EPS,RM,A1,B0,C1,C6
11*     10  FORMAT (I5,6F10.4,E15.6)
12*     WRITE (6,20) N,MU,EPS,RM,A1,B0,C1,C6
13*     20  FORMAT (1H0,10X,'NO. OF VELOCITIES',I8/11X,'REDUCED MASS',E15.6/
14*     1 11X,'WELL-DEPTH EPS',E15.6/11X,'POTENTIAL MINIMUM RM',E15.6/11X,
15*     2 'PHASE SHIFT COEFFICIENT A1',E15.6/11X,'BETA COEFFICIENT B0',
16*     3 E15.6/11X,'COEFFICIENT C1',E15.6/11X,'LONG RANGE C6',E15.6/)
17*     READ (5,30) (V(I),I=1,N)
18*     30  FORMAT (8F10.4)
19*     D1 = C6/HCROSS
20*     D2 = 2.*PI*RM*B0
21*     D3 = 4.*RM/HCROSS
22*     D4 = 2.*PI*RM*HCROSS/(EPS*C1)
23*     WRITE (6,40)
24*     40  FORMAT (//1H0,5X,'NO.', 8X,'V',13X,'QSL',10X,'DELQ',11X,'QTOT',
25*     1 10X,'DELQ/QSL'/4X,100(1H*))/)
26*     DO 200 I = 1,N
27*     QSL = 8.083*(D1/V(I))**0.4
28*     ETR = 0.5*MU*V(I)*V(I)
29*     Z = EPS/ETR
30*     PHI = - 0.75*PI + D3*EPS*(A1 + Z*(A(1) + Z*(A(2) + Z*(A(3) + Z*
31*     1 A(4))))/V(I)
32*     DELQ = D2*SQRT(D4*V(I))*(1. + H1*Z)*SIN(PHI)
33*     Q = QSL + DELQ
34*     QF = DELQ/QSL
35*     200 WRITE (6,50) I,V(I),QSL,DELQ,Q,QF
36*     50  FORMAT (3X,I5,5E15.6)
37*     GO TO 100
38*     END
```

ND OF COMPILATION: NO DIAGNOSTICS.

COMPILATION TIME: 0.653 SEC.

I/O REQUESTS: 50

I/O WORDS TRANSFERED: 57470

IV. PHASHT

The purpose of this program is to produce a fit of the experimental variable $Y = (N - \frac{3}{8})v_N$ to the model

$$Y = I + \frac{S_1}{E} + \frac{S_2}{E^2} + \dots \quad (\text{IV-1})$$

where, after regression, the following ansatz is made:

$$I = \frac{2a_1 \epsilon r_m}{\pi \hbar} \quad ; \quad S_i = \frac{2 \epsilon^{i+1} r_m}{\pi \hbar} A_i, \quad i=1,2,\dots \quad (\text{IV-2})$$

which leads to

$$\begin{aligned} a_1 \epsilon r_m &= \frac{\pi \hbar}{2} I \\ \epsilon^2 r_m &= \frac{\pi \hbar}{2} S_1 / A_1 \\ \epsilon &= \frac{A_1 S_2}{A_2 S_1} \end{aligned} \quad (\text{IV-3})$$

Values of $\epsilon^2 r_m$ and ϵ are calculated from (IV-2) assuming A_1, A_2, A_3, A_4 are given by (I-5). "ERROR" denotes 95% confidence interval halfwidths. The confidence intervals were calculated using first-order propagation of error,** and took the error in A_1, A_2, A_3, A_4 into account.

 ** I.e., if $y = f(x_1, x_2)$, then

$$\sigma_y^2 \simeq \left(\frac{\partial f}{\partial x_1}\right)^2 \sigma_{x_1}^2 + 2 \left(\frac{\partial f}{\partial x_1}\right) \left(\frac{\partial f}{\partial x_2}\right) \text{cov}(x_1, x_2) + \left(\frac{\partial f}{\partial x_2}\right)^2 \sigma_{x_2}^2$$

Input to the program is as follows:

Card 1: title information in columns 1-72 (18A4)

Card 2: NOB, IWGHT, MU (2I5, F10.4)

Card 3 (or more): V(I), I = 1, ..., NOB (8F10.4)

Card 4 (or more): INDEX(I), I = 1, ..., NOB (8F10.4)

where

NOB - number of observed extrema

IWGHT - if 0 data has assumed constant absolute error. If 1 ,
data is assumed to have constant relative error.

MU = μ (reduced mass)

V(I) - extrema velocity v_N for I-th extremum

INDEX(I) - extrema index N for I-th extremum

R,SI PHASHT

LE 000 COMPILED BY FOR-V S7E6 ON 04 JAN 72 AT 00:33:58

STORAGE USED: CODE(1) 000424; DATA(0) 000562

```
01 10 REAL INDEX (30),MU
03 20 DIMENSION X(30),Y(30),R(30),V(30),A(1),C(1),E(5),R(5,5),TITLE(10)
04 30 DATA A1/D.421559/,A/-0.1655,D.1067,-0.054,D.01397,CONS/1.4555476
04 40 1/.ERA1/D.9895E-4/,ERA1A2/1.6193E-2/
04 50 C READ IN EXPERIMENT TITLE
12 60 100 READ (5,5) (TITLE(1),I=1,10)
20 70 5 FORMAT (10A4)
21 80 WRITE (6,6) (TITLE(1),I=1,10)
27 90 6 FORMAT (1H1,10X,10A4/)
27 100 C READ IN NO. OF DATA POINTS NOB, WEIGHT SWITCH (WGHT (IF 0 ABSOLUT
27 110 C ERROR AND W(1) = 1. IF 1, RELATIVE ERROR AND W(1) = 1/Y(1)*0.2),
27 120 C AND REDUCED MASS MU.
27 130 C NOTE ... IF V IN UNITS OF KM/SEC AND MU IN 1.E-24 GRAM, THEN UNIT
27 140 C OF ENERGY WILL BE 1.E-14 ERGS. (NOTE THAT CONS HAS UNITS OF ACTIO
27 150 C 1.E-27 ERG-SEC)
30 160 READ (5,10) NOB, WGHT, MU
35 170 10 FORMAT (2I5,F10.4)
36 180 WRITE (6,20) NOB, WGHT, MU
43 190 20 FORMAT (1H0,10X,'NO. OF OBSERVATIONS ...',10/11X,'WEIGHTING SWIT
43 200 1H ...',10/11X,'REDUCED MASS ...',E15.6)
43 210 C READ IN EXTREMA VELOCITIES AND EXTREMA INDICES
44 220 READ (5,30) (V(1),I=1,NOB)
52 230 READ (5,30) (INDEX(1),I=1,NOB)
60 240 30 FORMAT (8F10.4)
61 250 WRITE (6,40)
63 260 40 FORMAT (17//5X,'NO.',6X,'V',15X,'ETR',11X,'INDEX',11X,'X',14X,'Y
63 270 1/6X,80(1H*)/)
64 280 DO 500 I = 1,NOB
67 290 ETR = 0.5*MU*V(1)*V(1)
70 300 X(1) = 1./ETR
71 310 Y(1) = (INDEX(1) - 0.375)*V(1)
72 320 W(1) = 1.
73 330 IF (WGHT .EQ. 1) W(1) = 1./(Y(1)*Y(1))
75 340 500 WRITE (6,50) I,V(1),ETR,INDEX(1),X(1),Y(1)
06 350 50 FORMAT (13X,15,5E15.6)
07 360 CALL POLFIT (X,Y,W,NOB,C,E,R,NDEG,SIG)
10 370 WRITE (6,60) NDEG,SIG
14 380 60 FORMAT (17/10X,'POLYNOMIAL OF DEGREE',15,' DETERMINED',10X,'RMS R
14 390 IDUAL ...',E15.87/11X,'TERM',5X,'COEFFICIENT',10X,'ERROR',5X,50
14 400 21H*)/)
15 410 NN = NDEG + 1
16 420 DO 400 I = 1,NN
21 430 J = 1-1
22 440 400 WRITE (6,70) J,C(1),E(1)
30 450 70 FORMAT (9X,15,E15.5,5X,E15.5)
31 460 AER = CONS*C(1)
32 470 EE = CONS*E(1)
33 480 EPSRM = AER/A1
34 490 EE2 = EE/A1
35 500 WRITE (6,80) AER,EE,EPSRM,EE2
43 510 80 FORMAT (1/10X,'A1*EPS*RM =',E12.5,2X,'(ERROR =',E12.5,' )'/10X,'EPS
43 520 RM FROM A1 = 0.421559 ...',E12.5,2X,'(ERROR =',E12.5,' )')
```



```

244 53*      IF (NDEG .EQ. 0) GO TO 100
246 54*      EER = CONS*C(2)/A(1)
247 55*      EE = ABS(CONS*E(2)/A(1))
250 56*      EPS = EER/EPARM
251 57*      EE2 = EPS*SQRT(R(1,1)/C(1)**2 + R(2,2)/C(2)**2 - 2.*R(1,2)/(C(1)*C
251 58*      12)) + ERA1)
252 59*      WRITE (6,85) EER,EE,EPS,EE2
260 60*      85  FORMAT(/10X,'EPS*EPS*RM =',E12.5,2X,'(ERROR =',E12.5,' )'/10X,'EP
260 61*      1 FROM A1 =0.421559 ...',E12.5,2X,'(ERROR =',E12.5,' )')
261 62*      IF (NDEG .EQ. 1) GO TO 100
263 63*      EPS = C(3)*A(1)/(C(2)*A(2))
264 64*      EE = EPS*SQRT(R(2,2)/C(2)**2 + R(3,3)/C(3)**2 - 2.*R(2,3)/(C(2)*
264 65*      1 C(3)) + ERA1A2)
265 66*      WRITE (6,90) EPS,EE
271 67*      90  FORMAT (/10X,'EPS =',E12.5,2X,'(ERROR =',E15.5,' )')
272 68*      GO TO 100
273 69*      END

```

END OF COMPILATION: NO DIAGNOSTICS.

COMPILATION TIME: 0.959 SEC.
 I/O REQUESTS: 61
 I/O WORDS TRANSFERED: 61198

A. POLFIT

This subroutine fits a polynomial

$$p(x) = \sum_{k=0}^M c_k x^k$$

to a set of N data points (x_i, y_i) , $1 \leq i \leq N$, by weighted forward regression. The criterion used to determine c_0, c_1, \dots, c_M is the minimization of the approximate variance of fit S^2 :

$$S^2 = \frac{1}{N-M-1} \sum_{i=1}^N w_i (y_i - p(x_i))^2$$

where w_i is the weight assigned to the i -th data point (if the variance of the i -th data point is σ_i^2 , then $w_i \propto 1/\sigma_i^2$).

The mechanics of the fit are performed by use of calculated orthogonal polynomials:

$$p(x) = \sum_{k=0}^M a_k P_k(x)$$

where the P_k 's satisfy $P_0(x) = 1$ and

$$P_{k+1}(x) = (x - u_k) P_k(x) - v_k P_{k-1}(x)$$

$$\sum_{i=1}^N w_i P_k(x_i) P_j(x_i) = \delta_{kj} D_k$$

The fit is continued until all terms whose contributions to the variance S^2 are significant at the 90% level (F-test) have been added.

CALL POLFIT (X, Y, W, N, C, E, R, M, SIG)

Input:

X(I) - abscissa x_i of the I-th data point

Y(I) - ordinate y_i of the I-th data point

W(I) - weight w_i of the I-th data point

N - no. of data points

Output:

C(I) - C_{i-1} , coefficient of x^{i-1} in final polynomial

E(I) - 95% confidence interval halfwidth of C(I), i.e., $t \sigma_I$

R(I,J) - covariance of C(I) and C(J) multiplied by t^2 ,
i.e., $t^2 \text{ cov } (I,J)$

M - degree of final fitted polynomial

SIG - S , standard error of fit where t is the critical value
of the student-t statistic for $\alpha = .05$ (Equal-Tails) and
N-M-1 degrees of freedom.

NOTE: Because of dimensioning, the program in its given form is limited
to $N \leq 21$ and $M \leq 4$.

OR,SI POLFIT
 CLE 000 COMPILED BY FOR-V S7E6 ON 04 JAN 72 AT 08:34:03.

STORAGE USED: CODE(1) 000662: DATA(0) 000323

```

101 1* SUBROUTINE POLFIT (X,Y,W,N,C,E,R,M,SIG)
101 2* C FITS A POLYNOMIAL OF DEGREE M (DETERMINED BY ROUTINE) TO A SET OF
101 3* C N POINTS (X(I),Y(I)) I=1,...,N.
101 4* C W(I) IS THE WEIGHT ASSIGNED TO POINT I. E.G. FOR ASSUMED CONSTANT
101 5* C ABSOLUTE ERROR, W(I) = 1., AND FOR ASSUMED CONSTANT PERCENTAGE
101 6* C ERROR, W(I) = 1./(Y(I)+Y(I)).
101 7* C THE POLYNOMIAL IS GIVEN BY P(X) = C(1) + ... C(M+1)*X**M
101 8* C E(I) IS THE 95 PERCENT CONFIDENCE INTERVAL HALFWIDTH OF C(I)
101 9* C R(I,J) IS THE COVARIANCE BETWEEN C(I) AND C(J), MULTIPLIED BY THE
101 10* C SQUARE OF THE CRITICAL VALUE OF THE STUDENT T STATISTIC
101 11* C THE DEGREE IS INCREASED UNTIL ALL TERMS SIGNIFICANT AT THE 90
101 12* C PERCENT LEVEL HAVE BEEN INCLUDED.
101 13* C THE POLYNOMIAL IS DETERMINED USING THE METHOD OF ORTHOGONAL
101 14* C POLYNOMIALS.
101 15* C AT EXIT FROM THE ROUTINE M WILL BE THE DETERMINED DEGREE OF THE
101 16* C POLYNOMIAL AND SIG WILL CONTAIN THE RMS RESIDUAL OF THE FIT
103 17* DOUBLE PRECISION U,V,A,B,VY,AYY,WAYY,SYN,T,WORK,P1,P2,SUM1,SUM2,
103 18* 1 SUM3,SUM4
104 19* DIMENSION X(1),Y(1),W(1),C(1),E(1),U(5),V(5),A(5),B(5,5),D(5),
104 20* 1 R(5,5),F90(25),T95(25)
105 21* EQUIVALENCE (VY,B(1,5)),(T,B(1,4)),(WAYY,B(1,3)),(SYN,B(2,5)),
105 22* 1 (WORK,B(2,4)),(AYY,B(3,5))
106 23* DATA T95/12.706,4.303,3.182,2.776,2.571,2.447,2.365,2.306,2.262,
106 24* 1 2.228,2.201,2.179,2.160,2.145,2.131,2.120,2.110,2.101,2.093,2.08
106 25* 2, 2.080,2.074,2.069,2.064,2.060/
110 26* DATA F90/39.86,8.53,5.54,4.54,4.06,3.78,3.59,3.46,3.36,3.28,3.23,
110 27* 1 3.18,3.14,3.10,3.07,3.05,3.03,3.01,2.99,2.97,2.96,2.95,2.94,2.93,
110 28* 2 2.92/
112 29* DATA V(1)/0.00/
114 30* DO 200 I = 1,4
117 31* II = I + 1
120 32* DO 100 J = 1,II
123 33* 100 B(1,J) = 0.00
125 34* B(5,1) = 0.00
126 35* 200 B(1,1) = 1.00
130 36* B(5,5) = 1.00
131 37* SUM1 = 0.00
132 38* SUM2 = 0.00
133 39* SUM3 = 0.00
134 40* VY = 0.00
135 41* DO 300 I = 1,N
140 42* T = W(I)
141 43* SUM1 = SUM1 + T
142 44* SUM2 = SUM2 + T*X(I)
143 45* T = T*Y(I)
144 46* SUM3 = SUM3 + T
145 47* 300 VY = VY + T*Y(I)
147 48* A(1) = SUM3/SUM1
150 49* D(1) = SUM1
151 50* U(1) = SUM2/SUM1
152 51* B(2,1) = - U(1)
153 52* AYY = 0.00

```

154	53*		VY = VY - A(1)*A(1)*D(1)
155	54*		I = 1
156	55*	500	I = I + 1
157	56*		IF (I .GT. 5) GO TO 1100
161	57*		II = I - 1
162	58*		SUM1 = 0.00
163	59*		SUM2 = 0.00
164	60*		SUM3 = 0.00
165	61*		SUM4 = 0.00
166	62*		DO 800 J = 1, N
171	63*		P1 = 1.00
172	64*		P2 = 0.00
173	65*		WORK = X(J)
174	66*		DO 700 K = 1, II
177	67*		T = (WORK - U(K))*P1 - V(K)*P2
200	68*		P2 = P1
201	69*	700	P1 = T
203	70*		T = W(J)*P1
204	71*		SUM1 = SUM1 + T*P1*WORK
205	72*		SUM2 = SUM2 + T*P2*WORK
206	73*		SUM3 = SUM3 + T*P1
207	74*	800	SUM4 = SUM4 + T*Y(J)
211	75*		D(1) = SUM3
212	76*		U(1) = SUM1/SUM3
213	77*		V(1) = SUM2/D(11)
214	78*		A(1) = SUM4/SUM3
215	79*		WAYY = A(1)*A(1)*D(1)
216	80*		AYY = AYY + WAYY
217	81*		IF (1.EQ.2) GO TO 1000
221	82*		B(1,1) = -U(11)*B(11,1) - V(11)*B(1-2,1)
222	83*		DO 900 J = 2, 11
225	84*	900	B(1,J) = B(11,J-1) - U(11)*B(11,J) - V(11)*B(1-2,J)
227	85*	1000	IDF = N-1
230	86*		SYN = DABS(VY - AYY)/IDF
231	87*		FP = WAYY/SYN
232	88*		IF (FP .GT. F90(IDF)) GO TO 500
234	89*	1100	MM = 1-1
235	90*		M = MM-1
236	91*		AYY = AYY - WAYY
237	92*		IDF = N-MM
240	93*		SYN = DABS(VY - AYY)/IDF
241	94*		DO 1600 K = 1, MM
244	95*		T = 0.00
245	96*		DO 1500 J = K, MM
250	97*	1500	T = T + A(J)*B(J,K)
252	98*	1600	C(K) = T
254	99*		COEF = SYN*T95(IDF)**2
255	100*		DO 2000 K = 1, MM
260	101*		DO 1900 J = K, MM
263	102*		T = 0.00
264	103*		DO 1800 L = J, MM
267	104*	1800	T = T + B(L,K)*B(L,J)/D(L)
271	105*		R(K,J) = T*COEF
272	106*	1900	R(J,K) = R(K,J)
274	107*	2000	E(K) = SQRT(R(K,K))
276	108*		SIG = SQRT(SYN)
277	109*		RETURN

300

110•

END

END OF COMPILATION:

NO DIAGNOSTICS.

COMPILATION TIME:

1.526 SEC.

I/O REQUESTS:

66

I/O WORDS TRANSFERED:

62865

B. EXAMPLES

Four example calculations are given.

1. Data of U. Buck, K. A. Köhler, H. Pauly, Z. Phys. 244, 180 (1971).

IWGHT = 1 (assumed constant relative error), so the rms residual

S for the fit is an estimate of the coefficient of variation of

the data. The value $S = 0.31\%$ is compatible with known experimental precision.

Examples 2-4 are based upon the synthetic data calculated from (IV-1)

with I, S_1, S_2, S_3, S_4 , given by (IV-2), with $\varepsilon = 8$ cpe, $r_m = 4 \text{ \AA}$,

$a_1 = 0.421559$. I.e.,

$$\hat{Y}_i = I + \frac{S_1}{E_i} + \frac{S_2}{E_i^2} + \frac{S_3}{E_i^3} + \frac{S_4}{E_i^4} \quad (1 \leq i \leq 13)$$

and $Y_i = \hat{Y}_i (1 + \delta)$ where δ is a normal distributed

random variable with mean 0 and variance σ^2 . In each case

IWGHT = 1, so the calculated value of S should approximate σ .

2. $Y = \hat{Y}$, i.e., $\sigma = 0$. Calculated $S = 0.0098\%$.

3. $\sigma = 0.5\%$. Calculated $S = .55\%$.

4. $\sigma = 0.25\%$. Calculated $S = 0.18\%$.

DATA OF U. BUCK, K.A. KOHLER, AND H. PAULY ; Z. PHYSIK 244 180 (1971)

NO. OF OBSERVATIONS ... 13
WEIGHTING SWITCH ... 1
REDUCED MASS342499+02

NO.	V	ETR	INDEX	X	Y
1	.234000+01	.937694+02	.500000+01	.106645-01	.108225+02
2	.207500+01	.737336+02	.550000+01	.135823-01	.106344+02
3	.188000+01	.605264+02	.600000+01	.165217-01	.105750+02
4	.170500+01	.497827+02	.650000+01	.200813-01	.104431+02
5	.154500+01	.408777+02	.700000+01	.244632-01	.102356+02
6	.141300+01	.341911+02	.750000+01	.292473-01	.100676+02
7	.130500+01	.291642+02	.800000+01	.342886-01	.995062+01
8	.120700+01	.249485+02	.850000+01	.400826-01	.980687+01
9	.112500+01	.216738+02	.900000+01	.461387-01	.970312+01
10	.104500+01	.187009+02	.950000+01	.534734-01	.953562+01
11	.968000+00	.160465+02	.100000+02	.623189-01	.931700+01
12	.910000+00	.141812+02	.105000+02	.705160-01	.921375+01
13	.855000+00	.125188+02	.110000+02	.798801-01	.908437+01

POLYNOMIAL OF DEGREE 3 DETERMINED
RMS RESIDUAL31262-02

TERM	COEFFICIENT	ERROR
0	.11338+02	.15915+00
1	-.55601+02	.14017+02
2	.52421+03	.34821+03
3	-.22900+04	.25523+04

A1*EPS*RM = .18782+02 (ERROR = .26364+00)
EPS*RM FROM A1 = 0.42155944553+02 (ERROR = .62538+00)

EPS*EPS*RM = .55653+03 (ERROR = .14030+03)
EPS FROM A1 = 0.42155912492+02 (ERROR = .29827+01)

EPS = .14762+02 (ERROR = .62868+01)

TEST DATA --- EPS = 8. --- RM = 4. --- NO ERROR

NO. OF OBSERVATIONS ... 13
WEIGHTING SWITCH ... 1
REDUCED MASS300000+02

NO.	V	ETR	INDEX	X	Y
1	.800000+00	.960000+01	.839090+01	.104167+00	.641272+01
2	.900000+00	.121500+02	.778734+01	.823045-01	.667111+01
3	.100000+01	.150000+02	.725479+01	.666667-01	.687979+01
4	.110000+01	.181500+02	.678422+01	.550961-01	.705014+01
5	.120000+01	.216000+02	.636708+01	.462963-01	.719049+01
6	.130000+01	.253500+02	.599584+01	.394477-01	.730710+01
7	.140000+01	.294000+02	.566407+01	.340136-01	.740470+01
8	.150000+01	.337500+02	.536633+01	.296296-01	.748699+01
9	.160000+01	.384000+02	.509803+01	.260117-01	.755685+01
10	.170000+01	.433500+02	.485533+01	.230681-01	.761656+01
11	.180000+01	.486000+02	.463495+01	.205781-01	.766790+01
12	.190000+01	.541500+02	.443412+01	.184612-01	.771232+01
13	.200000+01	.600000+02	.425049+01	.166667-01	.775097+01

POLYNOMIAL OF DEGREE 4 DETERMINED
RMS RESIDUAL97530-04

TERM	COEFFICIENT	ERROR
0	.81434+01	.10321-01
1	-.25576+02	.96037+00
2	.13067+03	.29574+02
3	-.54394+03	.36361+03
4	.11076+04	.15322+04

A1*EPS*RM = .13490+02 (ERROR = .17097-01)
EPS*RM FROM A1 = 0.42155932000+02 (ERROR = .40556-01)
EPS*EPS*RM = .25600+03 (ERROR = .96126+01)
EPS FROM A1 = 0.42155980000+01 (ERROR = .30107+00)
EPS = .79998+01 (ERROR = .16387+01)

TEST DATA --- EPS = 8. --- RM = 4. --- SIGMA = 0.005

NO. OF OBSERVATIONS ... 13
WEIGHTING SWITCH ... 1
REDUCED MASS300000+02

NO.	V	ETR	INDEX	X	Y
1	.800000+00	.960000+01	.826601+01	.104167+00	.631281+01
2	.900000+00	.121500+02	.780906+01	.823045-01	.669065+01
3	.100000+01	.150000+02	.721831+01	.666667-01	.684331+01
4	.110000+01	.181500+02	.674615+01	.550984-01	.700827+01
5	.120000+01	.216000+02	.628429+01	.462923-01	.709115+01
6	.130000+01	.253500+02	.598548+01	.394417-01	.729362+01
7	.140000+01	.294000+02	.568245+01	.340116-01	.743044+01
8	.150000+01	.337500+02	.531429+01	.296296-01	.740894+01
9	.160000+01	.384000+02	.511698+01	.260417-01	.758717+01
10	.170000+01	.433500+02	.487927+01	.230681-01	.765726+01
11	.180000+01	.486000+02	.464704+01	.205761-01	.768967+01
12	.190000+01	.541500+02	.446258+01	.184672-01	.776641+01
13	.200000+01	.600000+02	.426992+01	.166667-01	.778985+01

POLYNOMIAL OF DEGREE 3 DETERMINED
RMS RESIDUAL54587-02

TERM	COEFFICIENT	ERROR
0	.84388+01	.23523+00
1	-.44189+02	.15733+02
2	.44756+03	.29728+03
3	-.20993+04	.16483+04

A1*EPS*RM = .13979+02 (ERROR = .38967+00)
EPS*RM FROM A1 = 0.42155933161+02 (ERROR = .92436+00)
EPS*EPS*RM = .44231+03 (ERROR = .15748+03)
EPS FROM A1 = 0.42155913338+02 (ERROR = .43880+01)
EPS = .15858+02 (ERROR = .51957+01)

TEST DATA --- EPS = 8. --- RM = 4. --- SIGMA = 0.0025

NO. OF OBSERVATIONS ... 13
WEIGHTING SWITCH ... 1
REDUCED MASS300000+02

NO.	V	ETR	INDEX		Y
1	.800000+00	.960000+01	.838536+01	.104167+00	.640828+01
2	.900000+00	.121500+02	.780310+01	.823045-01	.668529+01
3	.100000+01	.150000+02	.727100+01	.666667-01	.689600+01
4	.110000+01	.181500+02	.680110+01	.550964-01	.706871+01
5	.120000+01	.216000+02	.636197+01	.462963-01	.718436+01
6	.130000+01	.253500+02	.598382+01	.394477-01	.729147+01
7	.140000+01	.294000+02	.566941+01	.340136-01	.741217+01
8	.150000+01	.337500+02	.535622+01	.296296-01	.747183+01
9	.160000+01	.384000+02	.511618+01	.260417-01	.758589+01
10	.170000+01	.433500+02	.485833+01	.230681-01	.762166+01
11	.180000+01	.486000+02	.464257+01	.205761-01	.768163+01
12	.190000+01	.541500+02	.443228+01	.184672-01	.770883+01
13	.200000+01	.600000+02	.425656+01	.166667-01	.776312+01

POLYNOMIAL OF DEGREE 3 DETERMINED
RMS RESIDUAL18440-02

TERM	COEFFICIENT	ERROR
0	.81921+01	.79429-01
1	-.28619+02	.53186+01
2	.18464+03	.10056+03
3	-.71384+03	.55802+03

A1*EPS*RM = .13571+02 (ERROR = .13158+00)
EPS*RM FROM A1 = 0.42155932192+02 (ERROR = .31212+00)

EPS*EPS*RM = .28646+03 (ERROR = .53236+02)
EPS FROM A1 = 0.42155988986+01 (ERROR = .15719+01)

EPS = .10101+02 (ERROR = .37469+01)

V. XTREMA

This main program produces a fit of the experimental variable

$Y = (N - \frac{3}{8})v_N$ to the model

$$Y = c_1 + \frac{c_2}{E} \left(A_1 + \frac{A_2 c_3}{E} + \frac{A_3 c_3^2}{E^2} + \frac{A_4 c_3^3}{E^3} \right) \quad (V-1)$$

where, after regression the following ansatz is made:

$$c_1 = 2a_1 \epsilon r_m / \pi \hbar; c_2 = 2\epsilon^2 r_m / \pi \hbar; c_3 = \epsilon \quad (V-2)$$

which lead to

$$\begin{aligned} a_1 \epsilon r_m &= \frac{\pi \hbar}{2} c_1 \\ \epsilon^2 r_m &= \frac{\pi \hbar}{2} c_2 \\ \epsilon &= c_3 \end{aligned} \quad (V-3)$$

The details of the fitting procedure are described in V.A (FIT).

The description of the input and output is the same as in Section IV.

SI XTREMA

000 COMPILED BY FOR-V S7E6 ON 16 SEP 71 AT 19:23:25.

ORAGE USED: CODE(1) 000317; DATA(0) 000464

```

1*      REAL INDEX (30),MU
2*      DIMENSION E(30),Y(30),W(30),V(30),TITLE(18)
3*      DATA A1/0.421559/
4*      C      READ IN EXPERIMENT TITLE
5*      100    READ (5,5) (TITLE(I),I=1,18)
6*      5      FORMAT (18A4)
7*      WRITE (6,6) (TITLE(I),I=1,18)
8*      6      FORMAT (1H1,10X,18A4/)
9*      C      READ IN NO. OF DATA POINTS NOB, WEIGHT SWITCH IWGHT (IF 0 ABSOLUTE
10*     C      ERROR AND W(1) = 1. IF 1, RELATIVE ERROR AND W(1) = 1/Y(1)**2),
11*     C      AND REDUCED MASS MU.
12*     C      NOTE ... IF V IN UNITS OF KM/SEC AND MU IN 1.E-24 GRAM, THEN UNITS
13*     C      OF ENERGY WILL BE 1.E-14 ERGS. (NOTE THAT CONS HAS UNITS OF ACTION
14*     C      1.E-27 ERG-SEC)
15*      READ (5,10) NOB,IWGHT,MU
16*      10     FORMAT (2I5,F10.4)
17*      WRITE (6,20) NOB,IWGHT,MU
18*      20     FORMAT (1H0,10X,'NO. OF OBSERVATIONS ...',I10/11X,'WEIGHTING SWITC
19*     1H ...',I10/11X,'REDUCED MASS ...',E15.6)
20*     C      READ IN EXTREMA VELOCITIES AND EXTREMA INDICES
21*      READ (5,30) (V(I),I=1,NOB)
22*      READ (5,30) (INDEX(I),I=1,NOB)
23*      30     FORMAT (8F10.4)
24*      WRITE (6,40)
25*      40     FORMAT (1///5X,'NO.',8X,'V',15X,'ETR',11X,'INDEX',11X,'Y'/6X,60I
26*     1 1H*)/)
27*      DO 500 I = 1,NOB
28*      E(I) = 0.5*MU*V(I)*V(I)
29*      Y(I) = (INDEX(I) - 0.375)*V(I)
30*      W(I) = 1.
31*      IF (IWGHT.EQ. 1) W(I) = 1./(Y(I)*Y(I))
32*      500    WRITE (6,50) I,V(I),E(I),INDEX(I),Y(I)
33*      50     FORMAT (3X,15,4E15.6)
34*      SIG = FIT (E,Y,W,NOB,A1ERM,ERAER,E2R,ERE2R,EPS,EREPS,RM,ERRM)
35*      WRITE (6,60) SIG
36*      60     FORMAT (1/10X,'RMS RESIDUAL OF FIT ...',E15.5/)
37*      EPSRM = A1ERM/A1
38*      EE = ERAER/A1
39*      WRITE (6,80) A1ERM,ERAER,EPSRM,EE
40*      80     FORMAT (1/10X,'A1*EPS*RM =',E12.5,2X,'(ERROR =',E12.5,' )'/10X,'EPS*
41*     1RM FROM A1 = 0.421559 ...',E12.5,2X,'(ERROR =',E12.5,' )')
42*      EPS2 = E2R/EPSRM
43*      EE = EPS2*SQRT( (ERE2R/E2R)**2 + (EE/EPSRM)**2 )
44*      WRITE (6,85) E2R,ERE2R,EPS2,EE
45*      85     FORMAT(1/10X,'EPS*EPS*RM =',E12.5,2X,'(ERROR =',E12.5,' )'/10X,'EPS
46*     1 FROM A1 =0.421559 ...',E12.5,2X,'(LOWER BOUND ON ERROR =',E12.5,
47*     2 ' )' )
48*      WRITE (6,90) EPS,EREPS
49*      90     FORMAT (1/10X,'EPS =',E12.5,2X,'(ERROR =',E12.5,' )')
50*      WRITE (6,95) RM,ERRM
51*      95     FORMAT (1/10X,'RM =',E12.5,2X,'(ERROR =',E12.5,' )' )
52*      GO TO 100

```

53•

END

END OF COMPILATION:

NO DIAGNOSTICS.

COMPILATION TIME:

0.731 SEC.

I/O REQUESTS:

51

I/O WORDS TRANSFERED:

55235

A. FIT

This subprogram performs the mechanics of the fit of (V-1), given data $E(I)$, $Y(I)$, $W(I)$, for $I = 1, \dots, N$, where $W(I)$ is the weight of the I -th data point. Initial estimates of c_2 and c_3 (80 and 5, resp.) are iteratively refined by bilinear regression of the first-order expansion

$$Y_i \simeq c_1 + \left(\frac{\partial Y}{\partial c_2} \right) \bigg|_{c_2^0, c_3^0} c_2 + \left(\frac{\partial Y}{\partial c_3} \right) \bigg|_{c_2^0, c_3^0} (c_3 - c_3^0) \quad (V-4)$$

where

$$\begin{aligned} \frac{\partial Y}{\partial c_2} &= \frac{1}{E} \left(A_1 + \frac{A_2 c_3}{E} + \frac{A_3 c_3^2}{E^2} + \frac{A_4 c_3^3}{E^3} \right) \\ \frac{\partial Y}{\partial c_3} &= \frac{c_2}{E^2} \left(A_2 + \frac{2A_3 c_3}{E} + \frac{3A_4 c_3^2}{E^2} \right) \end{aligned} \quad (V-5)$$

The iteration is continued until the rms residual converges to 1%.

$Z = \text{FIT}(E, Y, W, N, \text{AIERM}, \text{ERAEM}, \text{E2R}, \text{ERE2R}, \text{EPS}, \text{EREPS}, \text{RM}, \text{ERRM})$

returns $Z = S$ the rms residual and

$\text{AIERMS} = a_1 \epsilon r_m$, $\text{E2R} = \epsilon^2 r_m$, $\text{EPS} = \epsilon$, and

ERAEM , ERE2R , ERRM , the resp. 95% confidence interval halfwidths of these quantities.

SI FIT

000 COMPILED BY FOR-V S7E6 ON 16 SEP 71 AT 19:23:27.

ORAGE USED: CODE(1) 000304; DATA(0) 000167

```

1*      FUNCTION  FIT (E,Y,W,N,ALERM,ERAER,E2R,ERE2R,EPS,FREPS,RM,ERRM)
2*      C      PERFORMS ITERATIVE FITTING OF EXTREMA VALUES ...
3*      C      E(1) = TRANSLATIONAL ENERGY OF POINT 1
4*      C      Y(1) = (N-0.375)*V(1)      --- EXTREMA ORDINATE
5*      DIMENSION E(1),Y(1),W(1),X(30,2),C(3),ER(4),A(4)
6*      DATA A/-0.1655,0.1057,-0.0544,0.0139/,CONS/1.65654781/
7*      C      NOTE - CONS = PI*HCROSS/2.
8*      EPS = 5.
9*      E2R = 80.
10*     SIGP = 0.
11*     KOUNT = 0
12*     100    KOUNT = KOUNT + 1
13*     IF (KOUNT .GT. 10) GO TO 400
14*     DO 200 I = 1,N
15*     X(1,1) = (A(1) + EPS*(A(2) + EPS*(A(3) + EPS*(A(4)/(E(1))/E(1)))/
16*     1 E(1))/E(1)
17*     200    X(1,2) = E2R*(A(2) + EPS*(2.*A(3) + 3.*EPS*(A(4)/(E(1))/E(1)))/
18*     1 (E(1)*E(1))
19*     SIG = BILINR (X,Y,W,N,C,ER,RHO,30)
20*     EPS = EPS + C(3)
21*     E2R = C(2)
22*     DEL = SIG - SIGP
23*     SIGP = SIG
24*     IF (ABS(DEL) .GT. 0.01*SIG) GO TO 100
25*     300    ALERM = CONS*C(1)
26*     ERAER = CONS*ER(1)
27*     E2R = CONS*E2R
28*     ERE2R = CONS*ER(2)
29*     EREPS = ER(3)
30*     RM = E2R/(EPS*EPS)
31*     ERRM = RM*SQRT( 4.*(EREPS/EPS)**2 + (ERE2R/E2R)**2 - 4.*RHO*EREPS
32*     1*ERE2R/(EPS*E2R) )
33*     FIT = SIG
34*     RETURN
35*     400    WRITE (6,10)
36*     10     FORMAT (//10X,'*****FAILURE TO CONVERGE IN 10 ITERATIONS//')
37*     GO TO 300
38*     END

```

END OF COMPILATION: NO DIAGNOSTICS.

COMPILATION TIME: 0.644 SEC.

I/O REQUESTS: 50

I/O WORDS TRANSFERED: 54973

B. BILINR

Performs a weighted bilinear regression of the model

$$\hat{Y}_i = c_1 + c_2 X_{i1} + c_3 X_{i2}$$

Z = BILINR (X, Y, W, N, C, E, RHO, NDIM)

Input:

X(I,1) - X_{i1} , I-th value of first variable

X(I,2) - X_{i2} , I-th value of second variable

Y(I), W(I) - ordinate and weight of I-th data pt.

N - No. of data

NDIM-row dimension of X

Output:

C(J) - c_j , J-th parameter

E(J) - 95% confidence interval halfwidth of C(J)

RHO - r_{23} correlation coefficient between c_2 and c_3

Z = S rms residual of fit, calculated from

$$S^2 = \frac{1}{N-3} \sum_{i=1}^N w_i (Y_i - \hat{Y}_i)^2$$

```

53*      SIG2 = 0.00
54*      SUMY = 0.00
55*      DO 200 I = 1,N
56*      T = Y(I) - C(1) - C(2)*X(I) - C(3)*X(I+NDIM)
57*      SIG2 = SIG2 + W(I)*T*T
58*      SUMY = SUMY + W(I)*T
59*      C(1) = C(1) + SUMY/SUMW
60*      IDF = N-3
61*      SIG2 = SIG2/IDF
62*      BILINR = DSQRT(SIG2)
63*      T = T95(IDF)*BILINR
64*      E(2) = T*DSQRT(A11)
65*      E(3) = T*DSQRT(A22)
66*      E(1) = T*DSQRT( (1.00 + (A11*SUMX1*SUMX1 + 2.00*A21*SUMX1*SUMX2 +
67*      1 A22*SUMX2*SUMX2)/SUMW)/SUMW )
68*      RHO = A21/DSQRT(A11*A22)
69*      RETURN
70*      END

```

END OF COMPILATION: NO DIAGNOSTICS.

COMPILATION TIME: 1.094 SEC.
 I/O REQUESTS: 58
 I/O WORDS TRANSFERED: 58883

C. EXAMPLES

The four examples are the same as described in IV-B.

1. Note that $S = 0.31\%$
2. $S = 0.12 \times 10^{-5} \%$ (true 0%)
3. $S = 0.66\%$ (true 0.5%)
4. $S = 0.21\%$ (true 0.25%)

NO. OF OBSERVATIONS ... 13
 WEIGHTING SWITCH ... 1
 REDUCED MASS342499+02

NO.	V	ETR	INDEX	Y
1	.234000+01	.937694+02	.500000+01	.108225+02
2	.207500+01	.737336+02	.550000+01	.106344+02
3	.188000+01	.605264+02	.600000+01	.105750+02
4	.170500+01	.497827+02	.650000+01	.104431+02
5	.154500+01	.408777+02	.700000+01	.102354+02
6	.141300+01	.341911+02	.750000+01	.100676+02
7	.130500+01	.291642+02	.800000+01	.995062+01
8	.120700+01	.249485+02	.850000+01	.980687+01
9	.112500+01	.216738+02	.900000+01	.970312+01
10	.104500+01	.187009+02	.950000+01	.953562+01
11	.968000+00	.160465+02	.100000+02	.931700+01
12	.910000+00	.141812+02	.105000+02	.921375+01
13	.855000+00	.125188+02	.110000+02	.908437+01

RMS RESIDUAL OF FIT30755-02

A1*EPS*RM = .18748+02 (ERROR = .13757+00)
 EPS*RM FROM A1 = 0.42155944474+02 (ERROR = .32633+00)

EPS*EPS*RM = .56106+03 (ERROR = .57075+02)
 EPS FROM A1 = 0.42155912615+02 (LOWER BOUND ON ERROR = .12867+01)

EPS = .18831+02 (ERROR = .24142+01)

RM = .15822+01 (ERROR = .26027+00)

TEST DATA --- NEW TERMS -- NO ERROR -- EPS = 8. -- RM = 4.

NO. OF OBSERVATIONS ... 13
WEIGHTING SWITCH ... 1
REDUCED MASS300000+02

NO.	V	ETR	INDEX	Y
1	.800000+00	.960000+01	.839812+01	.641849+01
2	.900000+00	.121500+02	.779061+01	.667405+01
3	.100000+01	.150000+02	.725640+01	.688140+01
4	.110000+01	.181500+02	.678505+01	.705106+01
5	.120000+01	.216000+02	.636754+01	.719105+01
6	.130000+01	.253500+02	.599611+01	.730744+01
7	.140000+01	.294000+02	.566423+01	.740482+01
8	.150000+01	.337500+02	.536643+01	.748714+01
9	.160000+01	.384000+02	.509810+01	.755695+01
10	.170000+01	.433500+02	.485537+01	.761663+01
11	.180000+01	.486000+02	.463497+01	.766795+01
12	.190000+01	.541500+02	.443414+01	.771236+01
13	.200000+01	.600000+02	.425050+01	.775100+01

RMS RESIDUAL OF FIT12267-07

A1*EPS*RM = .13490+02 (ERROR = .59740-06)
EPS*RM FROM A1 = 0.42155932000+02 (ERROR = .14171-05)

EPS*EPS*RM = .25600+03 (ERROR = .21102-03)
EPS FROM A1 = 0.42155980000+01 (LOWER BOUND ON ERROR = .66039-05)

EPS = .80000+01 (ERROR = .15783-04)

RM = .40000+01 (ERROR = .12538-04)

TEST DATA --- EPS = 8. --- RM = 4. --- SIGMA = 0.005

NO. OF OBSERVATIONS ... 13
WEIGHTING SWITCH ... 1
REDUCED MASS300000+02

NO.	V	ETR	INDEX	Y
1	.800000+00	.960000+01	.826601+01	.631281+01
2	.900000+00	.121500+02	.780906+01	.669066+01
3	.100000+01	.150000+02	.721831+01	.684331+01
4	.110000+01	.181500+02	.674615+01	.700827+01
5	.120000+01	.216000+02	.628429+01	.709115+01
6	.130000+01	.253500+02	.598548+01	.729362+01
7	.140000+01	.294000+02	.568245+01	.743044+01
8	.150000+01	.337500+02	.531429+01	.740894+01
9	.160000+01	.384000+02	.511698+01	.758717+01
10	.170000+01	.433500+02	.487927+01	.765726+01
11	.180000+01	.486000+02	.464704+01	.768967+01
12	.190000+01	.541500+02	.446258+01	.776641+01
13	.200000+01	.600000+02	.426992+01	.778986+01

RMS RESIDUAL OF FIT66103-02

A1*EPS*RM = .13653+02 (ERROR = .32379+00)
EPS*RM FROM A1 = 0.42155932386+02 (ERROR = .76808+00)

EPS*EPS*RM = .30311+03 (ERROR = .12063+03)
EPS FROM A1 = 0.42155993591+01 (LOWER BOUND ON ERROR = .37312+01)

EPS = .98608+01 (ERROR = .79641+01)

RM = .31173+01 (ERROR = .38182+01)

TEST DATA --- EPS = 8. --- RM = 4. --- SIGMA = 0.0025

NO. OF OBSERVATIONS ... 13
WEIGHTING SWITCH ... 1
REDUCED MASS300000+02

NO.	V	ETR	INDEX	Y
1	.800000+00	.960000+01	.838536+01	.640828+01
2	.900000+00	.121500+02	.780310+01	.668529+01
3	.100000+01	.150000+02	.727100+01	.689600+01
4	.110000+01	.181500+02	.680110+01	.706871+01
5	.120000+01	.216000+02	.636197+01	.718436+01
6	.130000+01	.253500+02	.598382+01	.729147+01
7	.140000+01	.294000+02	.566941+01	.741217+01
8	.150000+01	.337500+02	.535622+01	.747183+01
9	.160000+01	.384000+02	.511618+01	.758589+01
10	.170000+01	.433500+02	.485833+01	.762166+01
11	.180000+01	.486000+02	.464257+01	.768163+01
12	.190000+01	.541500+02	.443228+01	.770883+01
13	.200000+01	.600000+02	.425656+01	.776312+01

RMS RESIDUAL OF FIT20544-02

A1*EPS*RM = .13495+02 (ERROR = .98363-01)
EPS*RM FROM A1 = 0.42155932013+02 (ERROR = .23333+00)

EPS*EPS*RM = .25410+03 (ERROR = .34287+02)
EPS FROM A1 = 0.42155979372+01 (LOWER BOUND ON ERROR = .10726+01)

EPS = .77712+01 (ERROR = .25466+01)

RM = .42075+01 (ERROR = .21990+01)

VI. QFIT

This main program directs a weighted nonlinear regression of the model

$$\hat{Q}(v) = \gamma_1 v^{-2/5} + \gamma_2 v^{1/2} \left[1 + \frac{H_1 \gamma_5}{E} \right] \sin \phi \quad (\text{VI-1})$$

where

$$\phi = -\frac{3\pi}{4} + \frac{\gamma_3}{v} + \frac{\gamma_4}{vE} \left(A_1 + \frac{A_2 \gamma_5}{E} + \frac{A_3 \gamma_5^2}{E^2} + \frac{A_4 \gamma_5^3}{E^3} \right) \quad (\text{VI-2})$$

and after regression the ansatz $\gamma_5 = \epsilon$ and (I-8) is made, leading to

$$\begin{aligned} C_6 &= \hbar (\gamma_1 / 8.083)^{5/2} \\ \gamma_m &= \hbar \gamma_4 / 4 \gamma_5^2 \\ a_1 &= \gamma_3 \gamma_5 / \gamma_4 \\ g_0 &= \gamma_5^{7/2} \gamma_2 / \hbar^2 (\pi \gamma_4 / 2)^{3/2} \\ \epsilon &= \gamma_5 \end{aligned}$$

(VI-3)

The regression is automatically repeated with initial values for $\gamma_1 - \gamma_5$ being the values obtained from the first regression, and a new adjustable parameter γ_6 being added to the model:

$$\hat{Q}(v) = \gamma_1 v^{-2/5} + \gamma_2 v^{1/2} \left[1 + \frac{H_1 \gamma_5}{E} \right] \sin \phi + \gamma_6 \quad (\text{VI-4})$$

After regression the ansatz

$$\gamma_6 = \frac{2\pi}{3} \frac{C_8}{C_6} \quad (\text{VI-5})$$

is made, leading to

$$C_8 = \frac{3\hbar}{2\pi} \gamma_6 \left(\frac{\gamma_1}{8.083} \right)^{5/2} \quad (\text{VI-6})$$

The required input is of the following form:

CARD 1: Title information (18A4)

CARD 2: N, MU, EPS, RM, A1, GO, C6, IWGHT (15,5F10.4,E15.6,15)

CARD 3 (or more): V(I), I = 1, ..., N (8F10.4)

CARD 4 (or more): Q(I), I = 1, ..., N (8F10.4)

where

N - Number of velocities at which cross sections are given

MU - μ , reduced mass of the system

EPS, RM, A1, GO, C6 - initial estimates for ε , r_m , a_1 , g_0 , C_6

IWGHT - if 0 data are assumed to have constant absolute error; if 1, constant relative error

V(I) - the I-th velocity observation

Q(I) - the I-th cross section observation.

If the scale of the Q's is not known, C_6 , C_8 and g_0 will be found finally to contain the same factor, but no other parameters will be affected.

Output of the program includes the values of $\gamma_1, \dots, \gamma_6$ with error intervals (denoted parameters 1-6), and the correlation matrix of the errors of $\gamma_1, \dots, \gamma_6$.

I QFIT

DDO COMPILED BY FOR-V STE6 ON 14 SEP 71 AT 09:22:29.

PAGE USED: CODE(1) 000272; DATA(0) 007340; BLANK COMMON(2) 000620

```
1* C A CONSISTENT SET OF UNITS FOR THIS PROGRAM IS ...
2* C 1.E-24 GM FOR MASS, 1.E-14 ERGS FOR ENERGY, ANGSTROMS FOR LENGTH
3* C AND KM/SEC FOR VELOCITY.
4* REAL MU
5* DOUBLE PRECISION R(36),X,PAR,ER,F(200),F2(200),BUP(6),BLOW(6)
6* DIMENSION X(1200),Q(200),W(200),PAR(6),ER(6)
7* COMMON V(200),E(200)
8* DATA BLOW/6*0.00/,BUP/1.00,1.02,5.01,2.04,1.04,1.08/
9* EXTERNAL XSECT,DXSECT
10* 100 READ (5,10) (Q(I),I=1,18)
11* 10 FORMAT (10A4)
12* WRITE (6,20) (Q(I),I=1,18)
13* 20 FORMAT (1H1,10X,18A4)
14* READ (5,30) N,MU,EPS,RM,A1,G0,C6,IWGT
15* C IF IWGT = 0, ASSUMED CONSTANT ERROR. IF IWGT = 1, ASSUMED
16* C CONSTANT RELATIVE ERROR.
17* C FOR A LENNARD-JONES 12-6 POTENTIAL A1 = 0.421559, G0 = 0.188299
18* C CRUDE INITIAL ESTIMATES FOR EPS AND RM MIGHT BE 5. AND 4., RESP.
19* 30 FORMAT (I5,5F10.4,E15.6,I5)
20* WRITE (6,35) N,MU,EPS,RM,A1,G0,C6,IWGT
21* 35 FORMAT (1H0,10X,'NO OF DATA POINTS',I8/11X,'REDUCED MASS',E15.6/
22* 1 11X,'INITIAL EPS',E15.6/11X,'INITIAL RM',E15.6/11X,'INITIAL A1',
23* 2 E15.6/11X,'INITIAL G0',E15.6/11X,'INITIAL C6',E15.6/11X,'WEIGHT IN
24* 3G SWITCH',I8/)
25* CALL TRIAL (PAR,C6,A1,G0,EPS,RM)
26* READ (5,40) (V(I),I=1,N)
27* READ (5,40) (Q(I),I=1,N)
28* 40 FORMAT (8F10.4)
29* DO 200 I = 1,N
30* W(I) = 1.
31* IF (IWGT .EQ. 1) W(I) = 1./(Q(I)*Q(I))
32* 200 E(I) = 0.5*MU*V(I)*V(I)
33* WRITE (6,60)
34* 60 FORMAT (// 'O FIT WITH 5 PARAMETERS (NO C8)' //)
35* CALL GASS59 (1,XSECT,DXSECT,N,W,Q,5,PAR,BUP,BLOW,1.D-3,1.D-3,1.D-6
36* 1, 20,R,ER,F,F2,X)
37* CALL FINAL (5,PAR,ER,R)
38* WRITE (6,70)
39* 70 FORMAT (// 'O FIT WITH 6 PARAMETERS (WITH C8)' //)
40* CALL GASS59 (1,XSECT,DXSECT,N,W,Q,6,PAR,BUP,BLOW,1.D-3,1.D-3,1.D-6
41* 1, 10,R,ER,F,F2,X)
42* CALL FINAL (6,PAR,ER,R)
43* GO TO 100
44* END
```

END OF COMPILATION: NO DIAGNOSTICS.

COMPILATION TIME: 0.664 SEC.

I/O REQUESTS: 51

I/O WORDS TRANSFERED: 55129

A. TRIAL

This subprogram converts initial estimates for ϵ , r_m , a_1 , g_0 and C_6 into initial estimates for $\gamma_1, \dots, \gamma_6$ (denoted by PAR(1) ... PAR(6).)

CALL TRIAL (PAR, C6, A1, GO, EPS, RM)

Input:

C6 - long-range C_6

A1 - a_1 (I-5c)

GO - g_0 (I-5a)

EPS - ϵ

RM - r_m

Output:

PAR(1) = γ_1 (I-8)

PAR(2) = γ_2 (I-8)

PAR(6) = γ_6 (VI-8)

I TRIAL

000 COMPILED BY FOR-V S7E6 ON 14 SEP 71 AT 09:22:46.

RAGE USED: CODE(1) 000102; DATA(0) 000035

```
1*      SUBROUTINE TRIAL (PAR,C6,A1,GO ,EPS,RM)
2*      DOUBLE PRECISION PAR
3*      DIMENSION PAR(1)
4*      DATA HCROSS/1.0545919/,PI/3.14159265/
5*      PAR(1) = 8.083*(C6/HCROSS)**0.4
6*      PAR(2) = (2.*PI*RM)*GO *SQRT(2.*PI*RM*HCROSS/EPS)
7*      PAR(3) = EPS
8*      PAR(4) = 4.*RM*EPS/HCROSS
9*      PAR(5) = EPS*PAR(4)
10*     PAR(4) = A1*PAR(4)
11*     PAR(6) = 0.
12*     RETURN
13*     END
```

END OF COMPILATION: NO DIAGNOSTICS.

```
COMPILATION TIME: 0.395 SEC.
I/O REQUESTS: 49
I/O WORDS TRANSFERED: 52841
```

B. FINAL

This subprogram takes the final values of $\gamma_1, \dots, \gamma_6$ and their errors, and outputs values and errors for $\varepsilon, a_1, r_m, C_6, g_0, a_1 \varepsilon r_m, \varepsilon^2 r_m, \beta$, and C_8 .

CALL FINAL (NP, PAR, ERR, R)

where:

NP - no. of parameters of fit (5 or 6)

PAR(I) - γ_i $1 \leq I \leq NP$

ERR(I) - 95% confidence interval halfwidth for PAR(I)

R(I,J) - correlation coefficient r_{ij} between PAR(I) and PAR(J),
stored as an NPxNP matrix.

T-FINAL

000 COMPILED BY FOR-V S7E6 ON 14 SEP 71 AT 09:22:49.

RAGE USED: CODE(1) 000540; DATA(0) 000177

```

1*      SUBROUTINE FINAL (NP,PAR,ERR,R)
2*      DOUBLE PRECISION PAR,ERR,R(1)
3*      DIMENSION PAR(1),ERR(1)
4*      DATA HCROSS/1.0545919/,PI/3.14159265/
5*      NN = NP + 1
6*      EPS = PAR(3)
7*      EREPS = ERR(3)
8*      A1 = PAR(4)*EPS/PAR(5)
9*      ERA1 = A1*SQRT((ERR(4)/PAR(4))**2 + (ERR(3)/PAR(3))**2 + (ERR(5)/
10* 1 PAR(5))**2 + 2.*R(3+3*NN)*ERR(3)*ERR(4)/(PAR(3)*PAR(4)) -2.*
11* 2 R(3+4*NN)*ERR(3)*ERR(5)/(PAR(3)*PAR(5)) -2.*R(4+4*NN)*ERR(4)*
12* 3 ERR(5)/(PAR(4)*PAR(5)) )
13*      RM = 0.25*PAR(5)*HCROSS/(PAR(3)*PAR(3))
14*      ERRM = RM*SQRT( 4.*(ERR(3)/PAR(3))**2 + (ERR(5)/PAR(5))**2 -4.*
15* 1 R(3+4*NN)*ERR(3)*ERR(5)/(PAR(3)*PAR(5)) )
16*      C6 = HCROSS*(PAR(1)/8.083)**2.5
17*      ERC6 = 2.5*C6*ERR(1)/PAR(1)
18*      GO = 8.*PAR(2)*PAR(3)**3.5/(HCROSS*HCROSS*(2.*PI*PAR(5))**1.5)
19*      ERGO = GO*SQRT((ERR(2)/PAR(2))**2+12.25*(ERR(3)/PAR(3))**2 +2.25*
20* 1 (ERR(5)/PAR(5))**2 + 7.*R(2+2*NN)*ERR(2)*ERR(3)/(PAR(2)*PAR(3))
21* 2 -3.*R(2+4*NN)*ERR(2)*ERR(5)/(PAR(2)*PAR(5))-10.5*R(3+4*NN)*ERR(3)
22* 3 *ERR(5)/(PAR(3)*PAR(5)) )
23*      WRITE (6,10)
24* 10  FORMAT (///10X,'TERM',8X,'VALUE',8X,'95 PERCENT HALFWIDTH'/5X,
25* 1 50(1H*))
26*      WRITE (6,20) C6,ERC6,GO,ERGO,EPS,EREPS,A1,ERA1,RM,ERRM
27* 20  FORMAT (10X,' C6 ',2E15.6/10X,' GO ',2E15.6/10X,' EPS',2E15.6/10X,
28* 1 ' A1 ',2E15.6/10X,' RM ',2E15.6)
29*      A1ERM = 0.25*HCROSS*PAR(4)
30*      ERAER = 0.25*HCROSS*ERR(4)
31*      WRITE (6,30) A1ERM,ERAER
32* 30  FORMAT (/8X,'A1*EPS*RM',E12.6,E15.6)
33*      E2R = 0.25*HCROSS*PAR(5)
34*      ERE2R = 0.25*HCROSS*ERR(5)
35*      WRITE (6,35) E2R,ERE2R
36* 35  FORMAT (/8X,'RM*EPS**2',E12.6,E15.6)
37*      IF (NP .LT. 6) RETURN
38*      BETA = 1.5*PAR(6)/PI
39*      ERBETA = 1.5*ERR(6)/PI
40*      WRITE (6,40) BETA,ERBETA
41* 40  FORMAT (/10X,'BETA',2E15.6)
42*      C8 = C6*BETA
43*      ERC8 = C8*SQRT((ERC6/C6)**2 + (ERBETA/BETA)**2 +2.*R(1+5*NN)*ERC6
44* 1 *ERBETA/(C6*BETA))
45*      WRITE (6,50) C8,ERC8
46* 50  FORMAT (/10X,' C8 ',2E15.6)
47*      RETURN
48*      END

```

END OF COMPILATION: NO DIAGNOSTICS.

C. XSECT/DXSECT

Subprogram which calculates $Q(v)$ given $\gamma_1, \dots, \gamma_6$ by means of (I-6) (XSECT), or $\partial Q(v)/\partial \gamma_i$, $1 \leq i \leq 6$ (DXSECT).

1. CALL XSECT (PAR, F, NOB, NP)

Input:

PAR(I) - γ_i $1 \leq I \leq NP$

NOB - No. of velocities v

NP - No. of parameters γ_i (= 5 or 6)

Output:

F(I) - $Q(v)$ for I-th velocity

2. CALL DXSECT (PAR, F, NOB, NP)

Input:

PAR(I), NOB, NP - as above

Output:

F(I,J) - (NOB X NP matrix) $\partial Q(V)/\partial \gamma_j$ for I-th velocity

I XSECT

000 COMPILED BY FOR-V S7E6 ON 14 SEP 71 AT 09:22:56.

RAGE USED: CODE(1) 000420; DATA(0) 000110; BLANK COMMON(2) 000620

```
1*      SUBROUTINE XSECT (PAR,F,NOB,NP)
2*      C      SUBROUTINE WHICH CALCULATES CROSS SECTIONS GIVEN VALUES
3*      C      OF THE FOLLOWING PARAMETERS ...
4*      C      PAR(1) = 8.083*(C6/HCROSS)**0.4
5*      C      PAR(2) = 2.*PI*RM*GO*SGRT(2.*PI*RM*HCROSS/EPS)
6*      C      PAR(3) = EPS
7*      C      PAR(4) = 4.*A1*EPS*RM/HCROSS
8*      C      PAR(5) = 4.*EPS*EPS*RM/HCROSS
9*      C      PAR(6) = 2.*PI*C8/(C6*3.)
10*     DOUBLE PRECISION PAR,F,A,H1,PI75,PHI,Z
11*     DIMENSION PAR(1),F(1),A(4)
12*     COMMON V(200),E(200)
13*     DATA A/-0.1655D0,0.1057D0,-0.544D-1,0.139D-1/
14*     DATA H1/3.267D0/,PI75/2.35519449D0/
15*     DO 100 I = 1,NOB
16*     Z = PAR(3)/E(I)
17*     PHI = -PI75 + (PAR(4) + PAR(5)*(A(1) + Z*(A(2) + Z*(A(3) + Z*A(4)))))/
18*     1 E(I))/V(I)
19*     100 F(I) = PAR(1)/V(I)**0.4 + PAR(2)*DSQRT(V(I))*(1.DD + H1*Z)*DSIN(PHI
20*     1) + PAR(6)
21*     RETURN
22*     ENTRY DXSECT (PAR,F,NOB,NP)
23*     C      ENTRY POINT WHICH RETURNS MATRIX OF DERIVATIVES OF MODEL WITH
24*     C      RESPECT TO PARAMETERS
25*     DO 500 I = 1,NOB
26*     F(I) = 1.DD/V(I)**0.4
27*     Z = PAR(3)/E(I)
28*     SUM = (A(1) + Z*(A(2) + Z*(A(3) + Z*A(4))))/E(I)
29*     PHI = -PI75 + (PAR(4) + PAR(5)*SUM)/V(I)
30*     SPHI = DSIN(PHI)
31*     CPHI = DCOS(PHI)
32*     ROOTV = SQRT(V(I))
33*     TERM = 1.DD + H1*Z
34*     PROD = ROOTV*TERM
35*     F(I+NOB) = PROD*SPHI
36*     F(I+2*NOB) = PAR(2)*ROOTV*(TERM*CPHI*PAR(5)*(A(2) + Z*(2.*A(3) +
37*     1 3.*Z*A(4)))/(E(I)*V(I)) + H1*SPHI)/E(I)
38*     PROD = PROD*PAR(2)*CPHI
39*     F(I+3*NOB) = PROD/V(I)
40*     IF (NP .EQ. 6) F(I+5*NOB) = 1.DD
41*     500 F(I+4*NOB) = PROD*SUM/V(I)
42*     RETURN
43*     END
```

END OF COMPILE: NO DIAGNOSTICS.

COMPILE TIME: 0.978 SEC.

I/O REQUESTS: 59

I/O WORDS TRANSFERED: 57954

D. GASS59/MAXLIK

This subprogram performs general nonlinear regression of NOB observations $Y(I)$, with weights $W(I)$, to the model

$$\hat{Y} = \hat{Y}(\theta_1, \dots, \theta_n)$$

This program is a reworked version of a program of the same name of the Univ. Wis. Computing Center.

1. CALL GASS59(IO, YMU, DYMU, NOB, W, Y, NP, TH, BUP, BLOW, EPS1, EPS2, EPS3, MAXIT, D, E, F, R, DELZ)

INPUT: IO - I/O parameter. If 0, no printing is done. If 1, only last iteration is printed. If 2, all printing is performed.

CALL YMU (TH, F, NOB, NP) - stores $\hat{Y}(I)$ in $F(I)$ $1 \leq I \leq NOB$

CALL DYMU (TH, DELZ, NOB, NP) - Stores $\partial \hat{Y}(I) / \partial \theta_j$ in $DELZ(I, J)$

$1 \leq I \leq NOB, 1 \leq J \leq NP$.

NOB - No. of observations

$Y(I)$ - I-th observed value

NP - n, No. of parameters $\theta_1, \dots, \theta_n$

TH(J) - J-th parameter value θ_j . Initially should be set to an estimate of θ_j .

BUP(J), BLOW(J) - Bounds set upon the allowable values of TH(J):

$BLOW(J) \leq TH(J) \leq BUP(J)$.

EPS1 - Stopping criterion for relative change in the sum of squared residuals (SSR) per iteration.

EPS2 - Stopping criterion for relative change in each parameter per iteration.

EPS3 - Stopping criterion for relative change in SSR from initial SSR.

MAXIT - Maximum allowed number of iterations (e.g. 20)

F,R - work vectors of size NOB

DELZ - work space of size NOB X NP

OUTPUT: TH(I) - determined value of θ_i

D(I,J) - (NP X NP matrix) determined value of correlation between θ_i and θ_j

E(I) - determined 95% confidence interval halfwidth for θ_i

2. CALL MAXLIK (IO, YMU, DYMU, NOB, W, Y, NP, TH, D, E, F, R, DELZ)

The iterative fitting of the θ vector is done between entry points GASS59 and MAXLIK; from entry point MAXLIK onwards, the statistics of the fit are determined. A call to MAXLIK calculates the statistics for the given θ vector, but does not determine the θ vector by means of a fit.

T GASS59

000 COMPILED BY FOR-V S7E6 ON 14 SEP 71 AT 09:23:02.

RAGE USED: CODE(1) 003321; DATA(0) 002626

```
1*      SUBROUTINE GASS59 (IO,YMU,DYMU,NOB,W,Y,NP,TH,BUP,BLOW,EPS1,EPS2,
2*      1 EPS3,MAXIT,D,E,F,R,DELZ)
3*      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
4*      REAL Y,W
5*      REAL STUDNT
6*      DIMENSION Y(1),W(1),TH(1),BUP(1),BLOW(1),D(1),E(1),O(20),A(400),
7*      1 P(20),PHI(20),TB(20),WTS(20),F(1),R(1),DELZ(1)
8*      DATA FLAM/1.D-2/,FNU/1.D1/
9*      NPSQ = NP*NP
10*     GA = FLAM
11*     IF (IO .EQ. 0) GO TO 50
12*     WRITE (6,1) NOB,NP
13*     1   FORMAT ('1 ENTRY TO GASS59'//10X,'FIT TO',I8,3X,'OBSERVATIONS'//10X
14*     1,'THERE ARE',I8,3X,'PARAMETERS IN THE MODEL'//)
15*     WRITE (6,2)
16*     2   FORMAT ('//5X,'INITIAL PARAMETER VALUES'//15X,'LOWER BOUND',9X,'PAR
17*     1AMETER VALUE',5X,'UPPER BOUND'//5X,TB(1H,1)/)
18*     WRITE (5,2001) (I,BLOW(I),TH(I),BUP(I),I=1,NP)
19*     50   ITER = 1
20*     SSQ = 0.D0
21*     CALL YMU(TH,F,NOB,NP)
22*     DO 100 I = 1,NOB
23*     R(I) = Y(I) - F(I)
24*     100   SSQ = SSQ + W(I)*R(I)*R(I)
25*     KOUNT = 1
26*     SSQINT = SSQ
27*     SSQB4 = SSQ
28*     IF (IO .NE. 0) WRITE (6,3) SSQ
29*     3   FORMAT ('//5X,'INITIAL SUM OF SQUARES',D20.10)
30*     IF (SSQ .LT. 1.D-50) RETURN
31*     150   CONTINUE
32*     IF (IO .GE. 2) WRITE (6,4) ITER,KOUNT
33*     4   FORMAT ('///5X,'AT ITERATION',I5,10X,'CUMULATIVE NO. FUNCTION CALLS
34*     1 MADE',I10)
35*     GA = GA*DSQRT(SSQ/SSQB4)/FNU
36*     SSQB4 = SSQ
37*     INTCNT = 0
38*     CALL DYMU(TH,DELZ,NOB,NP)
39*     NI = - NOB
40*     DO 650 I = 1,NP
41*     NI = NI + NOB
42*     II = (I-1)*NP
43*     IJ = I - NP
44*     NJ = - NOB
45*     DO 550 J = 1,I
46*     NJ = NJ + NOB
47*     IJ = IJ + NP
48*     JI = II + J
49*     SUMD = 0.D0
50*     DO 500 K = 1,NOB
51*     500   SUMD = SUMD + DELZ(NI+K)*DELZ(NJ+K)*W(K)
52*     D(JI) = SUMD
```

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53* 550 D(IJ) = SUMD
54* Q(I) = 0.00
55* DO 600 K = 1,N0B
56* 600 Q(I) = Q(I) + W(K)*DELZ(NI+K)*R(K)
57* II = II + I
58* IF (D(II) .LT. 1.0-50) D(II) = 1.0-50
59* 650 E(I) = DSORT(D(II))
60* 700 NI = - NP
61* DO 710 I = 1,NP
62* NI = NI + NP
63* IJ = I - NP
64* WTS(I) = 0.00
65* DO 710 J = 1,I
66* IJ = IJ + NP
67* JI = NI + J
68* TEMP = D(IJ)
69* A(IJ) = TEMP
70* 710 A(JI) = TEMP
71* CALL SYMQR (A,NP,NP,P,DELZ)
72* NI = -NP
73* DO 730 I = 1,NP
74* NI = NI + NP
75* DO 730 J = 1,NP
76* JI = NI + J
77* 730 WTS(J) = WTS(J) + DABS(DELZ(JI))*P(I)
78* MASTER = 1
79* 760 DPROD = 1.00
80* NI = - NP
81* DO 770 I = 1,NP
82* NI = NI + NP
83* IF (WTS(I) .GT. WTS(MASTER)) MASTER = I
84* DPROD = DPROD*D(NI+I)**(1./NP)
85* IJ = I - NP
86* DO 770 J = 1,I
87* IJ = IJ + NP
88* JI = NI + J
89* A(IJ) = D(IJ)/(E(I)*E(J))
90* 770 A(JI) = A(IJ)
91* IF (DPROD .LT. 1.0-50) DPROD = 1.0-50
92* WTSMT = WTS(MASTER)
93* DO 780 I = 1,NP
94* II = (I-1)*NP + I
95* P(I) = Q(I)/E(I)
96* PHI(I) = P(I)
97* IF (DABS(WTS(I)) .LT. 1.0-50) WTS(I) = 1.0-50
98* WTS(I) = WTSMT/WTS(I)
99* 780 A(II) = A(II) + GA*WTS(I)*DPROD/D(II)
100* CALL MATIN (A,NP,P,1,DET,PIVRAT)
101* IF (PIVRAT .LT. 1.0-16) GO TO 990
102* STEP = 1.00
103* SUM1 = 0.00
104* SUM2 = 0.00
105* SUM3 = 0.00
106* DO 790 I = 1,NP
107* SUM1 = P(I)*PHI(I) + SUM1
108* SUM2 = SUM2 + P(I)*P(I)
109* SUM3 = SUM3 + PHI(I)*PHI(I)

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110* 790 PHI(I) = P(I)
111* TEMP = SUM1/DSQRT(SUM2*SUM3)
112* IF (DABS(TEMP) .GT. 1.00) TEMP = 1.00
113* TEMP = 57.2957800*DACOS(TEMP)
114* IF (IO .LT. 2) GO TO 800
115* WRITE (6,6) DET,PIVRAT,TEMP
116* 6 FORMAT (/9X,'DETERMINANT',D20.10,5X,'RATIO OF PIVOTS',D20.10,
117* 19X,'ANGLE IN SCALED COORDINATES',F10.5)
118* 800 DO 810 I = 1,NP
119* 810 P(I) = PHI(I)*STEP/E(I)
120* ISW = 0
121* DO 820 I = 1,NP
122* TB(I) = TH(I) + P(I)
123* 820 IF (TB(I) .GT. BUP(I) .OR. TB(I) .LT. BLOW(I)) ISW = 1
124* IF (IO .LT. 2) GO TO 830
125* WRITE (6,7)
126* 7 FORMAT (/9X,'TEST POINT PARAMETER VALUES')
127* WRITE (6,2011) (TB(I),I=1,NP)
128* 830 IF (ISW .EQ. 1) GO TO 860
129* SUMB = 0.00
130* CALL YMU(TB,F,N0B,NP)
131* KOUNT = KOUNT + 1
132* DO 840 I = 1,N0B
133* R(I) = Y(I) - F(I)
134* 840 SUMB = SUMB + W(I)*R(I)*R(I)
135* IF (IO .GT. 1) WRITE (6,8) SUMB
136* 8 FORMAT (/9X,'TEST POINT SUM OF SQUARES',D20.10)
137* 850 IF (SUMB .LE. (1.00 + EPS1)*SSQ) GO TO 890
138* 860 IF (TEMP .GT. 3.01 .AND. GA .GT. 1.0-50) GO TO 880
139* 870 STEP = 0.500*STEP
140* INTCNT = INTCNT + 1
141* IF (INTCNT .GE. 36) GO TO 980
142* GO TO 800
143* 880 GA = GA*FNU
144* INTCNT = INTCNT + 1
145* IF (INTCNT .GE. 36) GO TO 980
146* GO TO 760
147* 890 DO 900 I = 1,NP
148* 900 TH(I) = TB(I)
149* SSG = SUMB
150* IF (IO .GE. 2) WRITE (6,10) GA
151* 10 FORMAT (/9X,'AT THE END OF THE REGRESSION, GAMMA IS',D20.10)
152* IF (EPS2 .LE. 0.00) GO TO 920
153* DO 910 I = 1,NP
154* IF (DABS(P(I)) .GT. DABS(TH(I)*EPS2)) GO TO 920
155* 910 CONTINUE
156* WRITE (6,11) EPS2
157* 11 FORMAT (/ 'ITERATION STOPS ... RELATIVE CHANGE IN EACH PARAMETER I
158* 15 LESS THAN',D20.10)
159* GO TO 999
160* 920 IF (DABS(SUMB -SSQB4) .GT. EPS1*SSQB4) GO TO 930
161* WRITE (6,12) EPS1
162* 12 FORMAT (/ 'ITERATION STOPS ... RELATIVE CHANGE IN SUM OF SQUARES I
163* 15 LESS THAN',D20.10)
164* GO TO 999
X *DIAGNOSTIC* THE TEST FOR EQUALITY BETWEEN NON-INTEGERS MAY NOT BE MEANINGFUL.
165* 930 IF (STEP .NE. 1.00) GO TO 970

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165*      DO 950 IDUB = 1,5
167*      DO 935 I = 1,NP
168*      TB(I) = TH(I) + P(I)
169*      IF (TB(I) .GT. BUP(I) .OR. TB(I) .LT. BLOW(I)) GO TO 970
170* 935    CONTINUE
171*      SUMB = 0.00
172*      CALL YMU(TB,DELZ,NOB,NP)
173*      KOUNT = KOUNT + 1
174*      DO 940 I = 1,NOB
175* 940    SUMB = SUMB + W(I)*(Y(I) - DELZ(I))**2
176*      IF ((1.00 + EPS1)*SUMB .GE. SSQ) GO TO 970
177*      DO 945 I = 1,NP
178* 945    TH(I) = TB(I)
179*      DO 950 I = 1,NOB
180*      R(I) = Y(I) - DELZ(I)
181* 950    F(I) = DELZ(I)
182*      IF (IO .LT. 2) GO TO 960
183*      WRITE (6,7)
184*      WRITE (5,2011) (TB(I), I=1,NP)
185*      WRITE (6,8) SUMB
186* 960    SSQ = SUMB
187* 970    CONTINUE
188*      ITER = ITER + 1
189*      IF (SSQ .LE. EPS3*SSQINT) GO TO 991
190*      IF (ITER - MAXIT) 150,150,992
191* 980    WRITE (6,13)
192* 13     FORMAT (///'0***SUM OF SQUARES CANNOT BE REDUCED TO SUM OF SQUARE
193*      'S AT LAST ITERATION-TERMINATION OCCURS'/)
194*      GO TO 999
195* 990    WRITE(6,14) DET,PIVRAT
196* 14     FORMAT(/'RATIO OF PIVOTS IS TOO SMALL'/, DETERMINANT', 5X,D20.10,
197*      '15X,'RATIO OF PIVOTS',D20.10)
198*      GO TO 999
199* 991    WRITE (6,15) EPS3
200* 15     FORMAT (/ 'ITERATION STOPS ... CHANGE IN SUM OF SQUARES (RELATIVE
201*      '1TO INITIAL VALUE) IS LESS THAN',D20.10)
202*      GO TO 999
203* 992    WRITE (6,16) MAXIT
204* 16     FORMAT (/ ' *****ITERATION TERMINATES-- NO. OF ITERATIONS EXCEEDS',
205*      '1I10)
206* 2001   FORMAT (I9,3D20.10)
207* 2011   FORMAT (5X,6D20.10)
208* 2012   FORMAT(/I10,6D20.10/(10X,6D20.10))
209*      GO TO 999
210*      ENTRY MAXLIK (IO,YMU,DYMU,NOB,W,Y,NP,TH,D,E,F,R,DELZ)
211*      NPSQ = NP*NP
212* 999    SUMW = 0.00
213*      CALL YMU(TH,F,NOB,NP)
214*      SSQ = 0.00
215*      IF (IO .GT. 1) WRITE (6,1011)
216*      DO 1000 I = 1,NOB
217*      SUMW = SUMW + W(I)
218*      R(I) = Y(I) - F(I)
219*      IF (IO .LE. 1) GO TO 1000
220*      TEMP = DSQRT(W(I))*R(I)
221*      WRITE (6,1019) I,Y(I),F(I),R(I),TEMP
222* 1000   SSQ = SSQ + W(I)*R(I)*R(I)

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223* 1011 FORMAT (1H1,5X,'NO.',8X,'OBSERVED',7X,'FINAL MODEL VALUES',8X,
224* 1'RESIDUAL',8X,'WEIGHTED RESIDUAL'/5X,100(1H*))
225* 1019 FORMAT (I9,4D20.10)
226* CALL DYMU(TH,DELZ,NOB,NP)
227* NI = -NOB
228* DO 1900 I = 1,NP
229* NI = NI + NOB
230* II = (I-1)*NP
231* NJ = - NOB
232* IJ = I - NP
233* DO 1900 J = 1,I
234* NJ = NJ + NOB
235* IJ = IJ + NP
236* JI = II + J
237* SUMD = 0.00
238* DO 1800 K = 1,NOB
239* 1800 SUMD = SUMD + W(K)*DELZ(NI+K)*DELZ(NJ+K)
240* A(IJ) = SUMD
241* 1900 A(JI) = SUMD
242* 2000 IDF = NOB - NP
243* IF (IDF .NE. 0) WRITE (6,1015)
244* 1015 FORMAT ('CORRELATION MATRIX')
245* DO 2100 I = 1,NPSQ
246* 2100 D(I) = A(I)
247* CALL MATIN (D,NP,A,0,DET,PIVRAT)
248* DO 2200 I = 1,NP
249* II = (I-1)*NP + I
250* IF (D(II) .LT. 1.0-50) D(II) = 1.0-50
251* 2200 E(I) = DSQRT(D(II))
252* NI = - NP
253* DO 2400 I = 1,NP
254* NI = NI + NP
255* IJ = I - NP
256* DO 2300 J = 1,I
257* JI = NI + J
258* IJ = IJ + NP
259* D(JI) = D(JI)/(E(I)*E(J))
260* 2300 D(IJ) = D(JI)
261* 2400 IF (IDF .NE. 0) WRITE (6,2007) I,(D(NI+J),J=1,I)
262* 2007 FORMAT (5X,'ROW',I5,9F12.6/(13X,9F12.6))
263* IF (IDF .NE. 0) WRITE (6,31) DET,PIVRAT
264* 31 FORMAT (/'DETERMINANT',D20.10,10X,'RATIO OF PIVOTS',D20.10)
265* IF (IDF .EQ. 0) GO TO 3000
266* SDEV = SSQ/IDF
267* TFACTR = STUDNT(IDF)
268* IF (IDF .NE. 0) WRITE (6,1014) SSQ,SDEV,IDF
269* 1014 FORMAT (///5X,'SUM OF SQ. RESIDUALS',D20.10/5X,'MEAN SQ. RESIDUALS
270* 1',D20.10,5X,'(FOR',I8,3X,'DEGREES OF FREEDOM)')
271* SDEV = DSQRT(SDEV)
272* IF (IDF .NE. 0) WRITE (6,2008) SDEV,TFACTR,SUMW
273* 2008 FORMAT (5X,'STANDARD ERROR OF ESTIMATE',D20.10,10X,'CRITICAL STUDE
274* 1NT-T VALUE',F10.3/5X,'SUM OF WEIGHTS',D20.10)
275* IF (IDF .NE. 0) WRITE (6,2009)
276* 2009 FORMAT (///5X,'NO.',7X,'PARAMETER VALUE',4X,'STANDARD ERROR',7X,
277* 1'CONFID. BAND HALF-WIDTH',5X,90(1H*))
278* DO 2500 I = 1,NP
279* TEMP = E(I)*SDEV

```



```

280*      E(I) = TEMP*TFACR
281*      2500 IF (IO .NE. 0) WRITE (6,2001) I,TH(I),TEMP,E(I)
282*      3000 IF (IO .EQ. 0 .OR. PIVRAT .LT. 1.D-12) RETURN
283*      DO 3100 I = 1,NP
284*      II = (I-1)*NP + I
285*      3100 Q(I) = A(II)
286*      CALL SYMQR (A,NP,NP,P,DELZ)
287*      NI = - NP
288*      DO 3200 I = 1,NP
289*      NI = NI + NP
290*      A(NI + I) = Q(I)
291*      IJ = I - NP
292*      DO 3200 J = 1,I
293*      IJ = IJ + NP
294*      3200 A(IJ) = A(NI+J)
295*      WRITE (6,2003)
296*      2003 FORMAT (//9X,'EIGENVALUES OF MOMENT MATRIX-FINAL ANALYSIS'/)
297*      WRITE (6,2011) (P(I),I=1,NP)
298*      RETURN
299*      END

```

END OF COMPILATION: 1 DIAGNOSTICS.

```

COMPILATION TIME: 4.829 SEC.
I/O REQUESTS: 124
I/O WORDS TRANSFERED: 94557

```

E. SYMQR

This program is a reworked version of a Univ. of Wis. Computing Center routine of the same name which computes the eigenvalues and eigenvectors of a $N \times N$ symmetric matrix A by means of the Q-R method.

CALL SYMQR (A, N, NDIM, EIG., VEC)

INPUT: A - matrix of which eigenset is to be found. (Only the lower triangle of A is used)

N - size of A

NDIM - dimensioned size of A

OUTPUT: EIG(I) - I-th largest eigenvalue of A

VEC(J,I) - (NDIM X N matrix) - J-th component of eigenvector I .

SYMQR

JO COMPILED BY FOR-V S7E6 ON 08 SEP 71 AT 10:43:42.

PAGE USED: CODE(1) 0015611 DATA(0) 001052

```

1*      SUBROUTINE SYMQR (A,N,NDIM,EIG,VEC)
2*      C      USES THE QR ALGORITHM ON SYMMETRIC MATRIX A TO OBTAIN EIGENVALUES
3*      C      NOTE THAT ONLY LOWER TRIANGLE OF A IS USED (AND DESTROYED)
4*      C      EIG = VECTOR OF EIGENVALUES IN DESCENDING ORDER
5*      C      VEC = MATRIX OF EIGENVECTORS IN ORDER OF EIGENVALUES
6*      C      IND = ERROR RETURN INDICATOR
7*      C      IF 0 NORMAL, 1 SUM OF EIGENVALUES NOT TRACE
8*      C      IF 2 SUM OF SQUARED EIG. NOT EQUAL TO NORM
9*      C      IF 3 BOTH OF ERRORS
10*     IMPLICIT DOUBLE PRECISION (A-H,O-Z)
11*     DIMENSION A(1),GAMMA(50),BETA(50),BETASQ(50),EIG(1),W(49),VEC(1)
12*     1,P(49),Q(49),IPOSV(50),IVPOS(50),IORD(50)
13*     EQUIVALENCE (IPOSV(1),GAMMA(1)),(IVPOS(1),BETA(1)),(IORD(1),BETASQ
14*     1(1)),(P(1),BETA(1)),(Q(1),BETA(1))
15*     IND = 0
16*     IF (N .EQ. 0) GO TO 560
17*     N1 = N - 1
18*     N2 = N - 2
19*     ENORM = 0.00
20*     TRACE = 0.00
21*     NJ = -NDIM
22*     DO 110 J = 1,N
23*     NJ = NJ + NDIM
24*     JJ = NJ + J
25*     DO 100 I = J,N
26*     IJ = NJ + I
27*     100   ENORM = ENORM + A(IJ)**2
28*     TRACE = TRACE + A(JJ)
29*     110   ENORM = ENORM - 0.500*A(JJ)**2
30*     ENORM = ENORM + ENORM
31*     GAMMA(I) = A(I)
32*     IF (N2) 280,270,120
33*     120   NRN = -NDIM
34*     DO 260 NR = 1,N2
35*     NRN = NRN + NDIM
36*     ISUB = NRN + NR + 1
37*     B = A(ISUB)
38*     S = 0.00
39*     DO 130 I = NR,N2
40*     130   S = S + A(NRN + I + 2)**2
41*     A(ISUB) = 0.00
42*     IF (S .LE. 0.00) GO TO 250
43*     140   S = S + B*B
44*     SGN = 1.00
45*     IF (B .GE. 0.00) GO TO 160
46*     150   SGN = -1.00
47*     160   SQRTS = DSQRT(S)
48*     D = 0.500*SGN/SQRTS
49*     TEMP = DSQRT(0.500 + B*D)
50*     W(NR) = TEMP
51*     A(ISUB) = TEMP
52*     D = D/TEMP

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```

53*      B = -SGN*SQRTS
54*      DO 170 I = NR,N2
55*      TEMP = D*A(NRN + I + 2)
56*      W(I+1) = TEMP
57*      170  A(NRN + I + 2) = TEMP
58*      WTAW = 0.00
59*      DO 220 I = NR,N1
60*      SUM = 0.00
61*      DO 180 J = NR,I
62*      IJ = J*NDIM + I + 1
63*      180  SUM = SUM + A(IJ)*W(J)
64*      II = I + 1
65*      IF (N1 .LT. II) GO TO 210
66*      190  DO 200 J = II,N1
67*      IJ = I*NDIM + J + 1
68*      200  SUM = SUM + A(IJ)*W(J)
69*      210  P(I) = SUM
70*      220  WTAW = WTAW + SUM*W(II)
71*      DO 230 I = NR,N1
72*      230  Q(I) = P(I) - WTAW*W(I)
73*      DO 240 J = NR,N1
74*      QJ = Q(J)
75*      WJ = W(J)
76*      DO 240 I = J,N1
77*      IJ = J*NDIM + I + 1
78*      240  A(IJ) = A(IJ) - 2.00*(W(I)*QJ + WJ*Q(II))
79*      250  BETA(NR) = B
80*      BETASQ(NR) = B*B
81*      260  GAMMA(NR+1) = A(1SUB + NDIM)
82*      270  IJ = N2*NDIM + N
83*      B = A(IJ)
84*      BETA (N-1) = B
85*      BETASQ(N-1) = B*B
86*      GAMMA(N) = A(IJ + NDIM)
87*      280  BETASQ(N) = 0.00
88*      DO 300 I = 1,N
89*      IJ = I - NDIM
90*      DO 290 J = 1,N
91*      IJ = IJ + NDIM
92*      290  VEC(IJ) = 0.00
93*      IJ = (I-1)*NDIM + 1
94*      300  VEC(IJ) = 1.00
95*      M = N
96*      SUM = 0.00
97*      NPAS = 1
98*      GO TO 400
99*      310  SUM = SUM + SHIFT
100*      COSA = 1.00
101*      G = GAMMA(1) - SHIFT
102*      PP = G
103*      PPBS = PP*PP + BETASQ(1)
104*      PPBR = DSQRT(PPBS)
105*      NJ = - NDIM
106*      DO 370 J = 1,M
107*      NJ = NJ + NDIM
108*      COSAP = COSA

```

DIAGNOSTIC THE TEST FOR EQUALITY BETWEEN NON-INTEGERS MAY NOT BE MEANINGFUL.

```

109*      IF (PPBS .NE. 0.00) GO TO 320
110*      SINA = 0.00
111*      SINA2 = 0.00
112*      COSA = 1.00
113*      GO TO 350
114* 320    SINA = BETA(J)/PPBR
115*      SINA2 = BETASQ(J)/PPBS
116*      COSA = PP/PPBR
117*      NT = J + NPAS
118*      IF (NT .GT. N) NT = N
119* 330    DO 340 I = 1,NT
120*      IJ = NJ + I
121*      TEMP = COSA * VEC(IJ) + SINA * VEC(IJ + NDIM)
122*      VEC(IJ + NDIM) = -SINA * VEC(IJ) + COSA * VEC(IJ + NDIM)
123* 340    VEC(IJ) = TEMP
124* 350    DIA = GAMMA(J+1) - SHIFT
125*      U = SINA2 * (G + DIA)
126*      GAMMA(J) = G + U
127*      G = DIA - U
128*      PP = DIA * COSA - SINA * COSAP * BETA(J)
129*      IF (J .NE. M) GO TO 360
130*      BETA(J) = SINA * PP
131*      BETASQ(J) = SINA2 * PP * PP
132*      GO TO 380
133* 360    PPBS = PP * PP + BETASQ(J+1)
134*      PPBR = DSQRT(PPBS)
135*      BETA(J) = SINA * PPBR
136* 370    BETASQ(J) = SINA2 * PPBS
137* 380    GAMMA(M+1) = G
138*      NPAS = NPAS + 1
139*      IF (BETASQ(M) .GT. 1.0 - 21) GO TO 410
140* 390    EIG(M+1) = GAMMA(M+1) + SUM
141* 400    BETA(M) = 0.00
142*      BETASQ(M) = 0.00
143*      M = M - 1
144*      IF (M .EQ. 0) GO TO 430
145*      IF (BETASQ(M) .LE. 1.0 - 21) GO TO 390
146* 410    A2 = GAMMA(M+1)
147*      R2 = 0.500 * A2
148*      R1 = 0.500 * GAMMA(M)
149*      R12 = R1 + R2
150*      DIF = R1 - R2
151*      TEMP = DSQRT(DIF * DIF + BETASQ(M))
152*      R1 = R12 + TEMP
153*      R2 = R12 - TEMP
154*      DIF = DABS(A2 - R1) - DABS(A2 - R2)
155*      IF (DIF .LT. 0.00) GO TO 420
156*      SHIFT = R2
157*      GO TO 310
158* 420    SHIFT = R1
159*      GO TO 310
160* 430    EIG(1) = GAMMA(1) + SUM
161*      DO 440 J = 1,N
162*      IPOSV(J) = J
163*      IVPOS(J) = J
164* 440    IORD(J) = J
165*      M = N

```

```

166*      GO TO 470
167*      450 DO 460 J = 1,M
168*          IF (EIG(J) .GE. EIG(J+1)) GO TO 460
169*          TEMP = EIG(J)
170*          EIG(J) = EIG(J+1)
171*          EIG(J+1) = TEMP
172*          ITEMP = IORD(J)
173*          IORD(J) = IORD(J+1)
174*          IORD(J+1) = ITEMP
175*      460 CONTINUE
176*      470 M = M - 1
177*          IF (M .NE. 0) GO TO 450
178*          IF (N1 .EQ. 0) GO TO 500
179*          NL = -NDIM
180*          DO 490 L = 1,N1
181*              NL = NL + NDIM
182*              NV = IORD(L)
183*              NP = IPOSV(NV)
184*              IF (NP .EQ. L) GO TO 490
185*              LV = IVPOS(L)
186*              IVPOS(NP) = LV
187*              IPOSV(LV) = NP
188*              NNP = (NP - 1)NDIM
189*          DO 480 I = 1,N
190*              IL = NL + I
191*              INP = NNP + I
192*              TEMP = VEC(IL)
193*              VEC(IL) = VEC(INP)
194*              480 VEC(INP) = TEMP
195*          490 CONTINUE
196*      500 ESUM = 0.00
197*          ESSQ = 0.00
198*          DO 550 NRR = 1,N
199*              K = N1
200*              510 K = K - 1
201*              IF (K .LE. 0) GO TO 540
202*              SUM = 0.00
203*              DO 520 I = K,N1
204*                  IL = (NRR - 1)NDIM + I + 1
205*                  IJ = (K-1)NDIM + I + 1
206*              520 SUM = SUM + VEC(IL)*A(IJ)
207*              SUM = SUM + SUM
208*              DO 530 I = K,N1
209*                  IL = (NRR - 1)NDIM + I + 1
210*                  IJ = (K-1)NDIM + I + 1
211*              530 VEC(IL) = VEC(IL) - SUM*A(IJ)
212*              GO TO 510
213*          540 ESUM = ESUM + EIG(NRR)
214*          550 ESSQ = ESSQ + EIG(NRR)**2
215*              TEMP = DABS(128.00*TRACE)
216*          *DIAGNOSTIC* THE TEST FOR EQUALITY BETWEEN NON-INTEGERS MAY NOT BE MEANINGFUL.
217*              IF ((DABS(TRACE - ESUM) + TEMP) = TEMP .NE. 0.00) IND = IND + 1
218*              TEMP = 256.00*ENORM
219*          *DIAGNOSTIC* THE TEST FOR EQUALITY BETWEEN NON-INTEGERS MAY NOT BE MEANINGFUL.
220*              IF ((DABS(ENORM - ESSQ) + TEMP) = TEMP .NE. 0.00) IND = IND + 2
221*              IF (IND .NE. 0) WRITE (6,86) IND
222*      86 FORMAT (10* PROBABLE ERROR IN SYMQR = ,15)

```

221° 560 RETURN
222° END

END OF COMPILATION: 3 DIAGNOSTICS.

COMPILATION TIME: 3.176 SEC.
I/O REQUESTS: 92
I/O WORDS TRANSFERED: 79676

SYMQR
018A-09/08-10143

F. MATIN

Program which solves the set of equations $AX = B$, and inverts A , by means of Gaussian elimination with no pivoting.

CALL MATIN (A, N, B, NB, DET, PIVRAT)

where:

A - N X N matrix of equations (replaced by A^{-1})

N - size of A

B - N X NB matrix of right-hand side of equations (replaced by solution matrix X)

NB - no. of different right-hand sides (if 0, B is ignored by routine)

DET - returned determinant of A

PIVRAT - set to ratio of minimum to maximum pivots ($-\log_{10} \text{PIVRAT}$ is approx. no. of decimal figures lost in the computations).

FOR I MATIN

YCLE 000 COMPILED BY FOR-V S6D1 ON 08 AUG 70 AT 18:34:36.

```

0101 1* SUBROUTINE MATIN (A,N,B,NB,DET,PIVRAT)
0103 2* IMPLICIT DOUBLE PRECISION (A-H,O-Z)
0104 3* DIMENSION A(1),B(1)
0105 4* AL = DABS(A(1))
0106 5* AU = AL
0107 6* DET = 1.00
0110 7* NK = - N
0111 8* DO 1000 K = 1,N
0114 9* NK = NK + N
0115 10* KK = NK + K
0116 11* PIVOT = A(KK)
0117 12* PIVRAT = DABS(PIVOT)
0120 13* IF (AL .GT. PIVRAT) AL = PIVRAT
0122 14* IF (AU .LT. PIVRAT) AU = PIVRAT
0124 15* DET = DET*PIVOT
0125 16* IF (PIVRAT .LT. 1.0-50) PIVOT = 1.0-50
0127 17* A(KK) = 1.00
0130 18* PIVOT = 1.00/PIVOT
0131 19* KI = K - N
0132 20* DO 100 I = 1,N
0135 21* KI = KI + N
0136 22* 100 A(KI) = A(KI) *PIVOT
0137 23* IF (NB .EQ. 0) GO TO 300
0141 24* KI = K - N
0143 25* DO 200 I = 1,NB
0146 26* KI = KI + N
0147 27* 200 B(KI) = B(KI) *PIVOT
0151 28* 300 DO 1000 J = 1,N
0154 29* IF (J .EQ. K) GO TO 1000
0156 30* JK = NK + J
0157 31* T = A(JK)
0160 32* A(JK) = 0.00
0161 33* JI = J - N
0162 34* KI = K - N
0163 35* DO 400 I = 1,N
0166 36* JI = JI + N
0167 37* KI = KI + N
0170 38* 400 A(JI) = A(JI) - A(KI)*T
0172 39* IF (NB .EQ. 0) GO TO 1000
0174 40* JI = J - N
0175 41* KI = K - N
0176 42* DO 500 I = 1,NB
0201 43* JI = JI + N
0202 44* KI = KI + N
0203 45* 500 B(JI) = B(JI) - B(KI)*T
0205 46* 1000 CONTINUE
0210 47* PIVRAT = AL/AU
0211 48* RETURN
0212 49* END

```

END OF COMPILATION:

NO DIAGNOSTICS.

G. STUDENT

This function returns the value of the student-t statistic for IDF degrees of freedom at the 95% level. (Equal-Tails).

$$T = \text{STUDENT (IDF)}$$

SI STUDNT

000 COMPILED BY FOR-V STE6 ON 08 SEP 71 AT 10:43:59.

ORAGE USED: CODE(1) 000070; DATA(0) 000052

```
1*      FUNCTION STUDNT (IDF)
2*      C      RETURNS 95 PERCENT STUDENT-T VALUE FOR IDF DEG. OF FREEDOM
3*      DIMENSION T(29)
4*      DATA T/12.706,4.303,3.182,2.776,2.571,2.447,2.365,2.306,2.262,2.22
5*      18,2.201,2.179,2.160,2.145,2.131,2.120,2.110,2.101,2.093,2.086,2.08
6*      20,2.074,2.069,2.064,2.060,2.056,2.052,2.048,2.045/
7*      IF (IDF .LT. 60) GO TO 100
8*      STUDNT = 1.960 + 2.4/IDF
9*      50      RETURN
10*     100     IF (IDF .LT. 30) GO TO 200
11*      STUDNT = 1.958 + 2.52/IDF
12*      GO TO 50
13*     200     IF (IDF .LE. 0) GO TO 300
14*      STUDNT = T(IDF)
15*      GO TO 50
16*     300     STUDNT = 1.E+30
17*      GO TO 50
18*      END
```

END OF COMPILATION: NO DIAGNOSTICS.

COMPILATION TIME:	0.282 SEC.
I/O REQUESTS:	46
I/O WORDS TRANSFERED:	56744

H. EXAMPLES

The example is 48 cross sections $Q(v)$ for $1 < E^* < 40$ generated by means of XSECT (see Sect. II) from a L-J (12,6) potential with $\epsilon = 13.3$ cpe, $r_m = 4.92 \text{ \AA}$ (intended to mimic Li-Hg), $\mu = 9.69925$ ppg., $g_o = 0.186299$, $a_1 = 0.421559$, $C_6 = 0.378 \times 10^6 \text{ cpe-\AA}^6$. ($\sigma = 0.25\%$)

1. True value of $\gamma_5 = 0$

(a) NP = 5 (No C_8)

(1) Note that the correlation between $\gamma_1(C_6)$ and the other parameters is small.

(2) The "STANDARD ERROR OF ESTIMATE" is 0.262%, which is compatible with the precision of the calculated $Q(v)$'s.

(b) NP = 6 (C_8 assumed present)

(1) STANDARD ERROR OF ESTIMATE IS 0.259%, no change from NP = 5, indicating γ_6 is not necessary to the fit.

(2) The correlation between γ_1 and γ_6 is high. (-0.98)

(3) The determined value of C_8 is not significantly different from zero.

(4) The precision of C_6 has decreased markedly.

2. True value of $\gamma_5 = 2$

(a) NP = 5 (C_8 assumed zero)

(1) STANDARD ERROR OF ESTIMATE = 0.388% (larger than before)

(2) Precision of C_6 is lower than before.

(b) NP = 6 (C_8 assumed present)

(1) STANDARD ERROR OF ESTIMATE = 0.260%, lowered from NP = 5.

- (2) C_8 is found to be significantly greater than zero.
- (3) C_6 still has comparatively low precision.

It is to be noted that the presence of C_8 , either real or imagined, results in an uncertainty in the value of C_6 .

TEST RUN ON O'BRIEN G'S -- FAST CROSS SECTION GENERATOR

NO OF DATA POINTS 48
REDUCED MASS .969925+01
INITIAL EPS .140000+02
INITIAL RM .470000+01
INITIAL A1 .440000+00
INITIAL G0 .190000+00
INITIAL C6 .378000+06
WEIGHTING SWITCH 1

FIT WITH 5 PARAMETERS (NO C8)

②

ENTRY TO GASS59

FIT TO 48 OBSERVATIONS
THERE ARE 5 PARAMETERS IN THE MODEL

INITIAL PARAMETER VALUES

	LOWER BOUND	PARAMETER VALUE	UPPER BOUND

1	.0000000000+000	.1346960506+004	.1000000000+009
2	.0000000000+000	.8368514457+001	.1000000000+003
3	.0000000000+000	.1400000000+002	.5000000000+002
4	.0000000000+000	.1099130943+003	.2000000000+005
5	.0000000000+000	.3494053018+004	.1000000000+005

INITIAL SUM OF SQUARES .6924430832-001

ITERATION STOPS ... RELATIVE CHANGE IN EACH PARAMETER IS LESS THAN .1000000000-002

CORRELATION MATRIX

26

ROW	1	1.000000				
ROW	2	-.125735	1.000000			
ROW	3	.119972	-.785788	1.000000		
ROW	4	.069570	-.619235	.774383	1.000000	
ROW	5	.101764	-.763495	.964803	.903321	1.000000

DETERMINANT .4639324922-022 RATIO OF PIVOTS .1051003265-005

SUM OF SQ. RESIDUALS	.2956066462-003		
MEAN SQ. RESIDUALS	.6874573167-005	(FOR	43 DEGREES OF FREEDOM)
STANDARD ERROR OF ESTIMATE	.2621940725-002	CRITICAL STUDENT-T VALUE	2.017
SUM OF WEIGHTS	.7377959458-004		

NO.	PARAMETER VALUE	STANDARD ERROR	CONFID. BAND HALF-WIDTH
-----	-----------------	----------------	-------------------------

1	.1346493596+004	.5161492449+000	.1040863958+001
2	.8849899637+001	.1875344627+000	.3781827452+000
3	.1399492168+002	.5074537144+000	.1023333511+001
4	.1047705400+003	.1596391954+000	.3219291409+000
5	.3369161074+004	.6615348134+002	.1334356660+003

EIGENVALUES OF MOMENT MATRIX-FINAL ANALYSIS

.6864768959-002	.5771285384-003	.2862986311-003	.2605084319-004	.1570056419-00
-----------------	-----------------	-----------------	-----------------	----------------

TERM

VALUE

95 PERCENT HALFWIDTH

C6 .377715+06 .729954+03

G0 .211935+00 .627958-01

EPS .139949+02 .102333+01

A1 .435199+00 .363346-01

RM .453529+01 .687149+00

A1*EPS*RM .276225+02 .848760-01

RM*EPS**2 .888272+03 .351800+02

FIT WITH 6 PARAMETERS (WITH C8)

ENTRY TO GASS59

FIT TO 48 OBSERVATIONS
THERE ARE 6 PARAMETERS IN THE MODEL

INITIAL PARAMETER VALUES

	LOWER BOUND	PARAMETER VALUE	UPPER BOUND

1	.0000000000+000	.1346493596+004	.1000000000+009
2	.0000000000+000	.8849899637+001	.1000000000+003
3	.0000000000+000	.1399492168+002	.5000000000+002
4	.0000000000+000	.1047705400+003	.2000000000+005
5	.0000000000+000	.3359161074+004	.1000000000+005
6	.0000000000+000	.0000000000+000	.1000000000+009

INITIAL SUM OF SQUARES .2956066462-003

ITERATION STOPS ... RELATIVE CHANGE IN EACH PARAMETER IS LESS THAN .1000000000-002

CORRELATION MATRIX

ROW	1	1.000000					
ROW	2	.109323	1.000000				
ROW	3	-.067173	-.787775	1.000000			
ROW	4	-.112322	-.520076	.775645	1.000000		
ROW	5	-.096477	-.767335	.964894	.904750	1.000000	
ROW	6	-.980106	-.136736	.092670	.128555	.118859	1.000000

DETERMINANT .1298484915-027 RATIO OF PIVOTS .1049823447-005

SUM OF SQ. RESIDUALS .2827158327-003
 MEAN SQ. RESIDUALS .6731329349-005 (FOR 42 DEGREES OF FREEDOM)
 STANDARD ERROR OF ESTIMATE .2594480555-002 CRITICAL STUDENT-T VALUE 2.013
 SUM OF WEIGHTS .7377959458-004

NO.	PARAMETER VALUE	STANDARD ERROR	CONFID. BAND HALF-WIDTH

1	.1343020206+004	.2573184744+001	.5192686754+001
2	.9835969663+001	.1873918117+000	.3731566717+000
3	.1398635876+002	.5053793366+000	.1019855490+001
4	.1047772472+003	.1596028352+000	.3220785173+000
5	.3370098131+004	.6609026839+002	.1333701501+003
6	.2118036661+001	.1541351037+001	.3110445357+001

5
EIGENVALUES OF MOMENT MATRIX-FINAL ANALYSIS

.6837116884-002 .5765694685-003 .2864523427-003 .9792655089-004 .7620278987-0

TERM	VALUE	95 PERCENT HALFWIDTH

C6	.375283+06	.362751+04
G0	.211061+00	.720543-01
EPS	.139864+02	.101986+01
A1	.434848+00	.408882-01
RM	.454211+01	.839337+00
A1*EPS*RM	.276243+02	.849153-01
RM*EPS**2	.888520+03	.351628+02
BETA	.101129+01	.148513+01
C8	.379520+06	.561013+06

TEST RUN ON O'BRIEN O'S --- WITH C8 = C6

NO OF DATA POINTS	48
REDUCED MASS	.969925+01
INITIAL EPS	.140000+02
INITIAL RM	.470000+01
INITIAL A1	.440000+00
INITIAL G0	.190000+00
INITIAL C6	.378000+06
WEIGHTING SWITCH	1

FIT WITH 5 PARAMETERS (NO C8)

7

ENTRY TO CASS59

FIT TO 48 OBSERVATIONS
THERE ARE 5 PARAMETERS IN THE MODEL

INITIAL PARAMETER VALUES

	LOWER BOUND	PARAMETER VALUE	UPPER BOUND
1	.0000000000+000	.1345900506+004	.1000000000+009
2	.0000000000+000	.8368514457+001	.1000000000+003
3	.0000000000+000	.1400000000+002	.5000000000+002
4	.0000000000+000	.1098130943+003	.2000000000+005
5	.0000000000+000	.3494053018+004	.1000000000+005

INITIAL SUM OF SQUARES .6944308972-001

ITERATION STEPS ... RELATIVE CHANGE IN SUM OF SQUARES IS LESS THAN .1000000000-002

CORRELATION MATRIX

ROW	1	1.000000				
ROW	2	-.125849	1.000000			
ROW	3	.120120	-.785519	1.000000		
ROW	4	.059694	-.619105	.774527	1.000000	
ROW	5	.101897	-.763207	.964780	.903471	1.000000

DETERMINANT .4538018739-C22 RATIO OF PIVOTS .1048084199-CC5

76

SUM OF SQ. RESIDUALS .6485054621-CC3

MEAN SQ. RESIDUALS .1508152237-004 (FOR

43 DEGREES OF FREEDOM)

STANDARD ERROR OF ESTIMATE .3883493578-CC2

CRITICAL STUDENT-T VALUE

2.017

SUM OF WEIGHTS .7339488055-004

NO. PARAMETER VALUE STANDARD ERROR CONFID. BAND HALF-WIDTH

1	.1346277770+004	.7663563823+000	.1545437330+001
2	.8842247107+001	.2781089456+000	.5608357880+000
3	.1401673648+002	.7529242141+000	.1519350458+001
4	.1047770373+003	.2372077541+000	.4783542557+000
5	.3372315152+004	.9828877413+002	.1982095972+003

EIGENVALUES OF MOMENT MATRIX-FINAL ANALYSIS

.6840167958-002 .5749404385-CC3 .2851315924-003 .2592519684-CC4 .1561022854-C

TERM

VALUE

95 PERCENT HALFWIDTH

C6 .377563+06 .106354+04

G0 .212611+00 .786564-01

EPS .140167+02 .151035+01

A1 .435497+00 .219404-01

RM .452542+01 .727141+00

A1*EPS*RM .276243+02 .126117+00

RM*EPS**2 .889104+03 .522576+02

FIT WITH 6 PARAMETERS (WITH C8)

ENTRY TO GASS59

FIT TO 48 OBSERVATIONS
THERE ARE 6 PARAMETERS IN THE MODEL

INITIAL PARAMETER VALUES

	LOWER BOUND	PARAMETER VALUE	UPPER BOUND
1	.0000000000+000	.1346277770+004	.1000000000+009
2	.0000000000+000	.8842247107+001	.1000000000+003
3	.0000000000+000	.1401673648+002	.5000000000+002
4	.0000000000+000	.1047770373+003	.2000000000+005
5	.0000000000+000	.3372315152+004	.1000000000+005
6	.0000000000+000	.0000000000+000	.1000000000+009

INITIAL SUM OF SQUARES .6485054621-003

ITERATION STOPS ... RELATIVE CHANGE IN SUM OF SQUARES IS LESS THAN .1000000000-002

CORRELATION MATRIX

ROW	1	1.000000					
ROW	2	.108430	1.000000				
ROW	3	-.066259	-.787424	1.000000			
ROW	4	-.111588	-.625830	.776739	1.000000		
ROW	5	-.095596	-.766952	.964858	.984885	1.000000	
ROW	6	-.980109	-.135852	.091774	.127835	.117993	1.000000

DETERMINANT .1264424246-027 RATIO OF PIVOTS .1046818301-005

SUM OF SQ. RESIDUALS .2834185229-003

MEAN SQ. RESIDUALS .6748060070-005 (FOR 42 DEGREES OF FREEDOM)

STANDARD ERROR OF ESTIMATE .2597702845-002

CRITICAL STUDENT-T VALUE 2.019

SUM OF WEIGHTS .7339488055-004

NO.	PARAMETER VALUE	STANDARD ERROR	CONFID. BAND HALF-WIDTH
-----	-----------------	----------------	-------------------------

1	.1342982568+004	.2582873877+001	.5212239424+001
2	.8828489430+001	.1878008742+000	.3789821599+000
3	.1401071320+002	.5067464533+000	.1022514331+001
4	.1047842052+003	.1602860629+000	.3234572713+000
5	.3373520804+004	.6634987007+002	.1338940363+003
6	.4127919393+001	.1547427233+001	.3122708120+001

EIGENVALUES OF MOMENT MATRIX-FINAL ANALYSIS

10

.6814585221-002	.5744860009-003	.2853441146-003	.9742674141-004	.7579928003-006
-----------------	-----------------	-----------------	-----------------	-----------------

TERM	VALUE	95 PERCENT HALFWIDTH
------	-------	----------------------

C6	.375257+06	.364102+04
G0	.211848+00	.724291-01
EPS	.140107+02	.102261+01
A1	.435184+00	.490069-01
RM	.453093+01	.838421+00
A1*EPS*RM	.276261+02	.852789-01
RM*EPS**2	.889422+03	.353009+02
BETA	.197094+01	.149099+01
C8	.739608+06	.566678+06

VII. JWKB

This main program computes JWKB phase shifts $\eta_l(E)$ for given reduced energies $E^* = E/e$ and values of the orbital quantum number l such that $b^* = (l + \frac{1}{2})/ka$ is a multiple of 0.05 (For details of the calculation of η_l , see function PHASHT).

The total cross section is given by

$$Q(E) = \frac{4\pi}{k^2} \sum_{l=0}^{\infty} (2l+1) \sin^2 \eta_l \quad (\text{VII-1})$$

Letting

$$\delta q_l = b \sin^2 \eta_l \quad (\text{VII-2})$$

and

$$q_L = \sum_{l=0}^L \delta q_l \quad (\text{VII-3})$$

Since $Q = \frac{8\pi}{k} q_{\infty}$, the program computes Q by means of

$$Q = \frac{8\pi}{k} (q_L + \Delta q_L) \quad (\text{VII-4})$$

where L is a value large enough so that $\Delta q_L = q_{\infty} - q_L$ can be estimated accurately.

Values of δq_l are calculated at every 0.05 in b^* until one of the following is true:

(1) $b^* > 2$ and $\delta Q = \frac{8\pi}{k} \delta q_l < 0.1 \text{ \AA}^2/b$ (This condition forces the remaining cross section ΔQ to be less than 0.05 \AA^2).

(2) The Jeffreys-Born long-range phase shift $\eta_L^{JB} = \frac{3\pi}{16} \frac{C_6}{\hbar v b} < 2$ and agrees with η_L to within 0.01 radians for 3 successive values of l .

When either condition is satisfied, this value of l is taken as L .

The intermediate values of η_L are then calculated by interpolation (DNTERP)*. The remaining cross section $\Delta Q = \frac{8\pi}{k} \Delta q_L$ is

* The program could be improved by replacement of DNTERP with a continued-fraction interpolation program, since the limiting form of η_L is $\propto 1/b$.

estimated two different ways:

$$(1) \Delta q_L = \frac{\eta_L}{\eta_L^{JB}} \int_L^\infty b \sin^2 \eta_L^{JB} dl \quad (QJBVAL) \quad (VII-5)$$

(The factor of η_L / η_L^{JB} is to correct for the discrepancy between η_L and η_L^{JB} .)

(2) $q_\infty = \lim_{l \rightarrow \infty} q_l$ is obtained by means of the ϵ -algorithm (EPSALG).

Finally, the apparent C_6 constant C_6^{app} is calculated by means of:

$$C_6^{app} = \frac{\hbar^2 k}{\mu} \left(\frac{Q}{8.083} \right)^{5/2} \quad (VII-6)$$

INPUT:

Card 1: Title (20A4)

Card 2: NE, MU (I5, F10.4)

Card 3: (ELIST(I), I = 1, NE) (10F8.0)

where:

NE - No. of energies (in reduced units) for which cross sections are to be calculated

MU - reduced mass of system in ppg.

ELIST(I) - I-th energy in reduced units

NOTE: In addition, a user defined function POTIN/POT is required (q.v.)

OUTPUT: The values of E , C_6 , and σ (zero of potential) are in reduced units. The quantities EUNIT = e and RUNIT = a are the reducing units of energy and distance returned by POTIN (q.v.): they should be of the order of ϵ and r_m , respectively.

For ℓ corresponding to every 0.05 in $b^* = (\ell + \frac{1}{2})/A$, the following are outputted:

L - ℓ

B - b^*

YO - $y_0 = 1/r_0$

RO - r_0 the outer most zero of $1 - b^2/r^2 - V(r)/E$ (in reduced units)

ETATAB(LL) - η_ℓ

ETAJB - η_{JB}^ℓ

DELQ - δq_ℓ (in reduced units)

IER - Error return from determination of turning point. If = 0, normal convergence. If $\neq 0$ turning point is incorrect (see REGFAL)

ISW - Error return from determination of η_ℓ . If = 0, normal convergence. If $\neq 0$, did not converge (see PHASHT).

A table of the above quantities is printed out, the units being those obtained treating EUNIT and RUNIT as dimensional units.

Finally, the ϵ -algorithm sequence of diagonal convergents (EPSVEC(I), I = 1,M) are printed out, M being the number of applications of the algorithm, and the convergents for q_∞ appearing at every other element (the first such appearance being the one used). The following are then printed out:

T - Execution time in seconds

$$\text{CROSS} - Q_L = \frac{8\pi}{k} q_L (A^2)$$

$$Q - q_L$$

$$Q_{JB} - Q_L + \Delta Q^{JB} \text{ from eq. (VII-5) } (A^2)$$

$$C6APP - C_6^{\text{app},JB} \text{ (cpe-} A^6)$$

ND - highest degree used in interpolation (see DIFTAB)

and finally,

$$\text{CROSS} - Q = \frac{8\pi}{k} q_\infty$$

$$\text{EPSVEC}(J) - q_\infty$$

$$C6APP - C_6^{\text{app}}$$

NOTE: Values of q outputted are in reduced units.

REMARKS: (1) A user-defined potential function POTIN/POT is required (q.v.)

(2) EUNIT and RUNIT are treated as dimensional units except for actual cross sections which are in A^2 .

(3) The subroutines TIMSET (in line 54) and TIMGET (in line 93) are specific to the UWCC Univac 1108, and set and read an internal clock. These functions are not necessary for execution of the program. Line 54 may be deleted and line 93 replaced with "600 CONTINUE"

(4) The convergence tolerances for the calculation of η_l , convergence to η_l^{JB} , and determination of the turning point, are given by EPS (absolute), TOLJB (relative/absolute), TOLYO (relative), in line 8.

(5) The phase shift calculations generally terminate at $b^* < 3$ and give a cross section which has limits of error $\pm 5A^{02}$.

JWKB

05/31/72-01:53:12 (,0)

JWKB

```

1. C PROGRAM WHICH COMPUTES JWKB PHASE SHIFTS AND TOTAL CROSS SECTIONS
2. C A CONSISTENT SET OF UNITS FOR THIS PROGRAM ARE
3. C ANGSTROMS, PICOPICOGRAMS, AND DECIPICOSECONDS (GIVING CENTIPICOERGS
4. C AS THE UNIT OF ENERGY)
5. REAL MU
6. DIMENSION ELIST(200), ETATAB(200), DIF(2000), EPSVEC(20)
7. COMMON B, RO, E, X
8. DATA EPS/0.005/, TOLJB/0.01/, TOLYO/1.E=5/
9. DATA PI2/1.57079633/, HX2/1.11216241/
10. EXTERNAL VEFF
11. WRITE (6,2) TOLYO, EPS, TOLJB
12. 2 FORMAT (1H1,5X,'ENTRY TO JWKB/DNTERP',///5X,'TOLERANCE FOR YO (RE
13. 1LATIVE)',E12.5/5X,'TOLERANCE FOR ETA (ABS)',E12.5/5X,'TOLERANCE FO
14. 2R JB LIMIT',E12.5)
15. C READ IN TITLE OF EXPERIMENT
16. READ (5,3) (DIF(I), I=1,20)
17. 3 FORMAT (20A4)
18. WRITE (6,5) (DIF(I), I=1,20)
19. 5 FORMAT (1H1,10X,20A4)
20. C READ IN NO. OF ENERGIES NE AND REDUCED MASS MU
21. READ (5,6) NE, MU
22. 6 FORMAT (15,F10.4)
23. C READ IN LIST OF ENERGIES
24. READ (5,7) (ELIST(I), I=1,NE)
25. 7 FORMAT (10F8.0)
26. C POTIN SHOULD RETURN THE VALUE OF THE ZERO OF THE POTENTIAL
27. C C6 SHOULD BE VALUE OF LONG-RANGE C6 IN REDUCED UNITS, THE
28. C SCALE OF WHICH ARE GIVEN IN EUNIT(ENERGY) AND RUNIT (LENGTH)
29. SIGMA = POTIN(C6,EUNIT,RUNIT)
30. SIGINV = 1./SIGMA
31. SIGIN2 = 2.*SIGINV
32. CONSJB = 0.1875*PI2*C6
33. ECONS = 2.*MU*EUNIT/HX2
34. WRITE (6,9) MU, C6, SIGMA, EUNIT, RUNIT
35. 9 FORMAT (///5X,'PHASE SHIFTS AND CROSS SECTIONS FOR REDUCED MASS',
36. 1 E14.6/5X,'LONG-RANGE C6',E14.6/5X,'ZERO OF POTENTIAL',E14.6/
37. 2 5X,'UNITS OF ENERGY AND LENGTH',2E14.6)
38. DO 1000 I = 1,NE
39. E = ELIST(I)
40. WAVE = SQRT(E*ECONS)
41. A = WAVE*RUNIT
42. CJB = CONSJB*A/E
43. COEF = 16.*PI2*RUNIT/WAVE
44. WRITE (6,10) E, WAVE, A
45. 10 FORMAT (///5X,'ENERGY',F10.5,5X,'WAVE NO.',E15.6,5X,'A=WAVE*RUNIT'
46. 1,E14.6//5X,'FOLLOWING TABLE IN REDUCED UNITS EUNIT,RUNIT'/)
47. WRITE (6,15)
48. 15 FORMAT (14X,'L',5X,'B',8X,'YO',10X,'RO',9X,'ETA',11X,'ETAJB',
49. 1 9X,'DELQ',7X,'IER',3X,'ISW'/5X,100(1H*)//)
50. IJB = 0
51. C CALCULATE PHASE SHIFTS AT EVERY .05 IN REDUCED IMPACT PARAMETER
52. LSTEP = A/20.
53. IF (LSTEP.LT.1) LSTEP = 1
54. CALL TIMSET(0.)
55. DO 500 LL = 1,200

```

```

56.      NETA = LL
57.      L = LSTEP*(LL-1)
58.      B = (L+0.5)/A
59.      IF (B .GT. SIGMA) GO TO 100
60.      XL = SIGINV
61.      XU = SIGIN2
62.      GO TO 200
63.  100   XL = 1./B
64.      XU = SIGINV
65.  C     FIND TURNING POINT Y0 = 1./RO
66.  C     IER = 0, NORMAL. IF NOT 0, ERROR IN ROOT (SEE REGFAL)
67.  200   CALL REGFAL(XL,XU,X,VEFF,TOL,Y0,5,20,IER)
68.      RO = 1./X
69.  C     CALCULATE PHASE SHIFT ETA
70.  C     ISW = 0, NORMAL. IF NOT 0, THEN DID NOT CONVERGE TO EPS ACCURACY
71.      TOL = EPS/A
72.      ETAJB = CJB/B**5
73.      IF (ETAJB .LT. 1.) TOL = ETAJB*TOL
74.      ETATAB(LL) = A*PHASHT(TOL,9,ISW)
75.      DELQ = B*(SIN(ETATAB(LL)))**2
76.      WRITE (6,20) L,B,X,RO,ETATAB(LL),ETAJB,DELQ,IER,ISW
77.  20    FORMAT (10X,15,3F10.6,3E14.6,2I6)
78.      IF (COEF*B*DELQ .GT. 0.1 .OR. B .LT. 2.) GO TO 400
79.      WRITE (6,22)
80.  22    FORMAT (/5X,'REMAINING CROSS SECTION IS LESS THAN 0.05 SQ ANG')
81.      GO TO 600
82.  400   TOL = TOLJB
83.      IF (ETAJB .LT. 1.) TOL = ETAJB*TOL
84.      IF (ABS(ETATAB(LL) - ETAJB) .LT. TOL ) IJB = IJB + 1
85.      IF (IJB .LT. 3 .OR. ETAJB .GT. 2.) GO TO 500
86.      WRITE (6,23) IJB
87.  23    FORMAT (/5X,'AFTER ',I8,5X,'ASYMPTOTIC PHASE SHIFTS, ETAJB IS LESS
88.      1THAN 1')
89.      GO TO 600
90.  500   CONTINUE
91.      WRITE (6,25)
92.  25    FORMAT (10X,'MORE THAN 200 PARTIAL WAVES ARE REQUIRED')
93.  600   T = TIMGET(0)
94.      ND = 10
95.      CALL DIFTAB(ETATAB,NETA,DIF,ND,EPS)
96.      NMAX = LSTEP*(NETA-1) + 1
97.      BSTEP = LSTEP/A
98.      BO = 0.5/A
99.      M = 0
100.     IEPS = 0
101.     Q = 0.
102.     DO 700 LL = 1,NMAX
103.     L = LL - 1
104.     B = (L+0.5)/A
105.     TOL = EPS
106.     ETAJB = CJB/B**5
107.     IF (ETAJB .LT. 1.) TOL = ETAJB*TOL
108.     ETA = DINTERP(B,BO,BSTEP,ETATAB,NETA,DIF,ND,TOL)
109.     DELQ = B*(SIN(ETA))**2
110.     Q = Q + DELQ
111.     IF (LL .LE. NMAX - 20 .OR. IEPS .EQ. 1) GO TO 700
112.     CALL EPSALG (Q,M,EPSVEC)

```



```

113.      J = 2 + 2*(M/2) = M
114.      IF (M .LE. 2) GO TO 700
115.      IF (ABS(EPSVEC(J) - EPSVEC(J+2)) * COEF .GT. 0.1) GO TO 700
116.      IEPS = 1
117.      WRITE (6,21) (EPSVEC(K),K=1,M)
118.  21    FORMAT (1/5X,'EPSILON ALGORITHM CONVERGES ...'/5X,10F11.4)
119.      GO TO 800
120.  700   CONTINUE
121.  800   B = B + 1./A
122.      QJB = Q + A*ETA*QJBVAL(CJB,B)/ETAJB
123.      CROSSJB = COEF*QJB
124.      CROSS = COEF*Q
125.      C6APP = HX2*WAVE*(CROSSJB/8.083)**2.5/MU
126.      WRITE (6,30) T,CROSS,Q,CROSSJB,QJB,C6APP,ND
127.  30    FORMAT (1/5X,'TIME (SEC)',F10.3/10X,'CROSS SECTION AT LAST PHASE S
128.      HIFT',F10.2,10X,'Q',F10.3/10X,'JB EXTRAPOLATED CROSS SECTION (SQ A
129.      2NG)',F10.2,10X,'QJB',F10.3,10X,'C6 APPARENT',E15.6/10X,'HIGHEST OR
130.      3DER DIFFERENCE USED IN INTERPOLATION',18)
131.      IF (M .EQ. 0) GO TO 1000
132.      CROSS = COEF*EPSVEC(J)
133.      C6APP = HX2*WAVE*(CROSS/8.083)**2.5/MU
134.      WRITE (6,40) CROSS,EPSVEC(J),C6APP
135.  40    FORMAT (10X,'EPSILON ALGORITHM CROSS SECTION',F10.2,10X,'Q',F10.3,
136.      1 10X,'C6 APPARENT',E14.6)
137.  1000  CONTINUE
138.      STOP
139.      END

```

NO OF COMPILATION: NO DIAGNOSTICS.

A. PHASHT

This function computes the value of the JWKB phase shift η_l for given E and $b = (l + \frac{1}{2})/k$, to a given absolute tolerance, by means of the formulae

$$\begin{aligned}\eta_l &= \eta_1 + \eta_2 \quad (b > r_0) \\ \eta_l &= \frac{\pi}{2} b - r_0 - \int_0^{y_0} \frac{1-F^{1/2}}{y^2} dy \quad (b \leq r_0)\end{aligned}\quad (\text{VII-7})$$

where $V(r)$ is the potential, r_0 is the largest positive zero of $F(r)$

$$F(r) = 1 - \frac{b^2}{r^2} - \frac{V(r)}{E}$$

and $y = 1/r$ ($y_0 = 1/r_0$). The quantities η_1 and η_2 are given by

$$\begin{aligned}\eta_1 &= \int_{1/b}^{y_0} \frac{F^{1/2}}{y^2} dy \\ \eta_2 &= \int_0^{1/b} \frac{F^{1/2} - \sqrt{1-b^2 y^2}}{y^2} dy\end{aligned}\quad (\text{VII-8})$$

The integrals are performed by function ADSIMP (q.v.)

CALL: ETA = PHASHT (EPS, NITER, ISW)

INPUT: EPS - Absolute error tolerance for integrals in Eq. (VII-7,8)

NITER - 2^{NITER} is the maximum number of points which may be used in the integrations.

OUTPUT: ISW - = 0, Normal convergence of integrations; if $\neq 0$, integrals
did not converge (see ADSIMP)

PHASHT - value of η_l (b,E)

NOTE: Values of $B(b)$, $RO(r_o)$, and $YO(y_o)$ are obtained through the
COMMON statement of line 10.

M PHASHT

9-05/31/72-01153117 (1,0) PHASHT

```
1. FUNCTION PHASHT (EPS,NITER,ISW)
2. C FINDS VALUE OF JWKB PHASE SHIFT FOR IMPACT PARAMETER B, TURNING
3. C POINT RO, EPS IS ABS ERROR CRITERION. 2**NITER IS MAX NO. OF
4. C POINTS WHICH MAY BE USED IN INTEGRATION (NITER, LE, 9)
5. C IF ISW .NE. 0, FAILED TO CONVERGE TO ACCURACY EPS
6. C NOTE - REQUIRES FUNCTIONS F,F2,F3, WHICH FOR Y = 1/R RETURN
7. C F(Y) = (1-SQRT(1-(B*Y)**2 - V(R)/E))/(Y*Y)
8. C F2(Y) = SQRT(1-(B*Y)**2-V(R)/E)/(Y*Y)
9. C F3(Y) = (SQRT(1-(B*Y)**2-V(R)/E)-SQRT(1-(B*Y)**2))/(Y*Y)
10. COMMON B,RO,E,YO
11. DATA PI2/1.57079633/
12. EXTERNAL F,F2,F3
13. LIMIT = 2**NITER
14. IF (B .LE. RO) GO TO 100
15. BINV = 1./B
16. TOL = 0.5*EPS
17. ETA1 = ADSIMP(BINV,YO,F2,TOL,LIMIT,ISW1)
18. ETA2 = ADSIMP(0.,BINV,F3,TOL,LIMIT,ISW2)
19. ISW = ISW1 + ISW2
20. PHASHT = ETA1 + ETA2
21. RETURN
22. 100 PHASHT = PI2*B = RO*ADSIMP(0.,YO,F,EPS,LIMIT,ISW)
23. RETURN
24. END
```

END OF COMPILATION: NO DIAGNOSTICS.

B. VEFF/F/F2/F3

Four entry-point function which returns values of

$$VEFF(y) = 1 - b^2 y^2 - V(r)/E$$

$$F(y) = (1 - \sqrt{VEFF})/y^2$$

$$F2(y) = \sqrt{VEFF} / y^2$$

$$F3(y) = (\sqrt{VEFF} - \sqrt{1 - b^2 y^2}) / y^2$$

where $y = 1/r$, and b and E are obtained via the COMMON statement of line 2.

CALLS $Z = VEFF(X)$

$Z = F(X)$

$Z = F2(X)$

$Z = F3(X)$

ARGUMENT: $X = y$

```

1 F
2=05/31/72=01153:15 (,0) F
1. FUNCTION VEFF(X)
2. COMMON B,R0,E,Y0
3. U = B*X
4. VEFF = 1. = U*U = POT(1./X)/E
5. RETURN
6. ENTRY F(X)
7. IF (X .LT. 1.E-3) GO TO 200
8. U2 = X*X
9. V = POT(1./X)/E
10. WORK = B*B*U2 + V
11. IF (WORK .LT. 0.01) GO TO 100
12. IF (WORK .GT. 0.9999999 .AND. WORK .LT. 1.01) WORK = 0.9999999
13. VEFF = (1. = SQRT(1. = WORK))/U2
14. RETURN
15. 100 VEFF = 0.5*(B*B+V/U2)*(1. + 0.25*WORK*(1. + 0.5*WORK))
16. RETURN
17. 200 VEFF = 0.5*B*B
18. RETURN
19. ENTRY F2(X)
20. U = B*X
21. WORK = 1. = U*U = POT(1./X)/E
22. IF (WORK .LT. 0. .AND. WORK .GT. 0.01) WORK = WORK
23. VEFF = SQRT(WORK)/(X*X)
24. RETURN
25. ENTRY F3(X)
26. IF (X .LT. 1.E-3) GO TO 400
27. U2 = X*X
28. BB = B*B
29. DODA = BB + POT(1./X) / (U2*E)
30. WORK = U2*DODA
31. IF (WORK .LT. 0.01) GO TO 300
32. VEFF = (SQRT(ABS(1.=WORK))=SQRT(ABS(1.=BB*U2)))/U2
33. RETURN
34. 300 WORK = DODA*DODA
35. V = BB*BB
36. VEFF = 0.5*(BB-DODA) + 0.125*U2*(-(V-WORK) + 0.5*U2*(BB*V-WORK*
37. 1 DODA))
38. RETURN
39. 400 VEFF = 0.
40. RETURN
41. END

```

ND OF COMPILATION:

NO DIAGNOSTICS.

C. POTIN/POT

This function is a user-defined routine which returns values of potential constants (POTIN) and values of $V(r)$ (POT)

1. POTIN

CALL: SIGMA = POTIN (C6,EUNIT, RUNIT)

OUTPUT: C6 - values of C_6 in reduced units EUNIT = e and RUNIT = a

EUNIT - e dimensional unit in cpe of energy (of order ϵ)

RUNIT - a dimensional unit in \AA of distance (of order r_m or σ)

POTIN - returns value of σ ($V(\sigma) = 0$) in units of RUNIT

2. POT

CALL: V = POT(R)

INPUT: R = r in reduced units

OUTPUT: POT - $V(r)$ in reduced units

3. SAMPLE PROGRAM

The program listing is of a function which reads in a pointwise potential ($EUNIT = \epsilon$ and $RUNIT = r_m$). The value of $V(r)$ is calculated by quadratic interpolation

$$V(r) \simeq V + Ar + Br^2 \quad (VII-9)$$

where $A(I)$ and $B(I)$ are calculated by the routine. Extrapolation to low r is done by extrapolation of the closest quadratic, extrapolation to large r is done by

$$V(r) \simeq -\frac{C_6}{r^6} - \frac{C_8}{r^8} \quad (VII-10)$$

where $C_8 = C_8$ is calculated from the last data point and C_6 .

INPUT: Card 1: NOB (I5)

Card 2: EPS, RM, C6, SIGMA (10F8.3)

Card 3ff: (X(I), V(I), I = 1,NOB) (10F8.3)

where

NOB - no. of points

EPS - ϵ (cpe)

RM - r_m^0 (Å)

C6 - C_6 (reduced units)

SIGMA - σ (reduced units)

X(I) - I-th value of r (reduced units)

V(I) - I-th value of V (reduced units)

REMARKS: (1) C_8 is calculated from $C_8 = -r^8 V - r^6 C_6$ for $r = X(\text{NOB})$,

$$V = V(\text{NOB})$$

(2) It is not necessary that $\text{EPS} = \epsilon$ and $\text{RM} = r_m$, but any scale factors may be used.

```

POT
05/31/72=01:53:25 (.0) POT
1.      FUNCTION POTIN(C6CONS, EPS, RM)
2.      DIMENSION X(50), V(50), A(50), B(50)
3.      READ (5, 10) NOB
4.      10  FORMAT (I5)
5.      READ (5, 20) EPS, RM, C6, SIGMA
6.      C6CONS = C6
7.      20  FORMAT (10F8.3)
8.      READ (5, 20) (X(I), V(I), I=1, NOB)
9.      R2 = X(NOB)*X(NOB)
10.     R6 = R2*R2*R2
11.     C8 = -R2*(V(NOB)*R6 + C6)
12.     R2 = 1./X(NOB-1)**2
13.     R6 = R2*R2*R2
14.     TEST = -R6*(R2*C8 + C6)/V(NOB-1)
15.     NN = NOB - 1
16.     DO 90 I = 2, NN
17.     H1 = X(I) - X(I-1)
18.     H2 = X(I+1) - X(I)
19.     HH = X(I+1) - X(I-1)
20.     D12 = V(I) - V(I-1)
21.     D23 = V(I+1) - V(I)
22.     H12 = H1/H2
23.     A(I) = (H12*D23 + D12/H12)/HH
24.     90  B(I) = (H12*D23 - D12)/(H1*HH)
25.     NN = (NOB+1)/2
26.     RUP = X(NOB)
27.     POTIN = SIGMA
28.     RETURN
29.     ENTRY POT(R)
30.     IF (R .GT. RUP) GO TO 500
31.     I = NN
32.     100 IF (R .GT. X(I)) GO TO 200
33.     I = (I+1)/2
34.     IF (I .GT. 1) GO TO 100
35.     I = 2
36.     GO TO 400
37.     200 I = I + 1
38.     IF (I .EQ. NOB) GO TO 300
39.     IF (R=X(I)) 400, 400, 200
40.     300 I = NOB - 1
41.     400 HH = R - X(I)
42.     POTIN = V(I) + HH*(A(I)+HH*B(I))
43.     RETURN
44.     500 R2 = 1./(R-R)
45.     R6 = R2*R2*R2
46.     POTIN = -R6*(R2*C8+C6)
47.     RETURN
48.     END

```

ID OF COMPILATION; NO DIAGNOSTICS.

D. QJBVAL

Function which computes $\int_b^\infty b' \sin^2 \eta_l^{JB} db'$ where
 the integral is done by expansion of \sin^2 and $\eta_l^{JB} = \frac{3\pi}{32} \frac{C_6 A}{E b^5}$

CALL: Q = QJBVAL (CJB,B)

INPUT: CJB - $3\pi AC_6/32E$

B - b

OUTPUT: QJBVAL - $\int_b^\infty b' \sin^2 \eta_l^{JB} db'$

REMARKS: The value returned is correct to more than 3 significant figures for values of B for which $\eta_l^{JB} \leq 2$.

QJBVAL

05/31/72-01153127 (1,0)

QJBVAL

```
1.      FUNCTION QJBVAL(CJB,B)
2.      C      PERFORMS INTEGRAL FROM B TO INFINITY OF B*(SIN ETAJB)**2
3.      C      WHERE ETAJB IS J=B PHASE SHIFT FOR LONG-RANGE C6
4.      C      ETAJB = CJB/B**5, CJB = 3*PI*C6/(32*E)
5.      DIMENSION S(10)
6.      DATA S/1.,0.33333333,0.04444444,0.031746031E-2,0.14109347E-3
7.      1 =.42755597E-5,.93968345E-7,.15661391E-8,.20472406E-10,
8.      2 =.21549902E-12/
9.      QJBVAL = 0.
10.     T = B*B
11.     Z = CJB/(T*T)
12.     Z = Z*Z
13.     T = Z/T
14.     DODA = 1.
15.     DO 500 I = 1,10
16.     DELQ = S(I)*DODA/(10*I-2)
17.     QJBVAL = QJBVAL + DELQ
18.     IF (ABS(DELQ) .LT. 1.E-3*QJBVAL) GO TO 600
19.     500 DODA = DODA*T
20.     600 QJBVAL = Z*QJBVAL
21.     RETURN
22.     END
```

ID OF COMPILATION:

NO DIAGNOSTICS.

E. DNTERP

This function performs finite difference interpolation based on a difference table constructed by DIFTAB (q.v.) The appropriate formula (Forward, Backward, or Stirling's central difference) is used with maximum order such that:

(1) The order is less than or equal to the size of the difference table.

(2) The size of the next term to be added is less than the propagated error.

CALL: VALUE = DNTERP (X, XO, H, N, D, ND, EPS)

ARGUMENTS: X - abscissa of interpolant

XO - left-most abscissa of data

H - stepsize of data

Y(I) - I-th ordinate of data

D - difference table from DIFTAB (q.v.)

ND - highest-order difference available in D (returned by DIFTAB, q.v.)

EPS - estimate of the absolute error of a.Y(I)

OUTPUT: DNTERP - value of interpolated ordinate corresponding to X .

REMARK: The program extrapolates beyond the range of the data by means of the nearest forward/backwards difference polynomial. (This could be improved by extrapolating the difference table.)

1 DINTERP

1-05/31/72-01153:18 (,0) DINTERP

```

1.      FUNCTION DINTERP(X,X0,H,Y,N,D,ND,EPS)
2.      C      PERFORMS DIFFERENCE INTERPOLATION UP TO ORDER ND
3.      C      D = DIFFERENCE TABLE FROM DIFTAB
4.      C      EPS = ESTIMATE OF ABSOLUTE ERROR IN Y'S
5.      DIMENSION Y(1),D(1)
6.      M = 0
7.      DODA = 1.
8.      TOL = EPS
9.      THETA = (X-X0)/H
10.     I = THETA + 0.5
11.     IF (I .LT. 0) I = 0
12.     IF (I .GE. N) I = N - 1
13.     THETA = THETA - I
14.     I = I + 1
15.     DINTERP = Y(I)
16.     IF (I .GT. N - ND) GO TO 2000
17.     IF (I .LT. ND) GO TO 1000
18.     C      USE STIRLING'S CENTRAL DIFFERENCE FORMULA
19.     DO 400 J = 1,ND
20.     TOL = 2.*TOL
21.     L = J/2
22.     K = M + I - L
23.     IF (ABS(D(K)) .LE. TOL) GO TO 500
24.     DODA = DODA/J
25.     IF (2*L .NE. J) GO TO 300
26.     TERM = THETA*DODA
27.     DODA = DODA*(THETA-L)
28.     GO TO 350
29.     300    DODA = DODA*(THETA+L)
30.     DINTERP = DINTERP + 0.5*DODA*(D(K) + D(K+1))
31.     GO TO 400
32.     350    DINTERP = DINTERP + TERM*D(K)
33.     400    M = M + N - J
34.     500    RETURN
35.     C      USE NEWTON'S FORWARD DIFFERENCE FORMULA
36.     1000   DO 1500 J = 1,ND
37.     TOL = 2.*TOL
38.     K = M + I
39.     IF (ABS(D(K)) .LE. TOL) GO TO 1600
40.     DODA = DODA*(THETA-J+1)/J
41.     DINTERP = DINTERP + DODA*D(K)
42.     1500   M = M + N - J
43.     1600   RETURN
44.     C      USE NEWTON'S BACKWARDS DIFFERENCE FORMULA
45.     2000   DO 2500 J = 1,ND
46.     TOL = 2.*TOL
47.     K = M + I - J
48.     IF (ABS(D(K)) .LE. TOL) GO TO 2600
49.     DODA = DODA*(THETA+J-1)/J
50.     DINTERP = DINTERP + DODA*D(K)
51.     2500   M = M + N - J
52.     2600   RETURN
53.     END

```

END OF COMPILATION:

NO DIAGNOSTICS.

F. DIFTAB

This program constructs a finite difference table from N equally-spaced data points, with ordinates y_i ($1 \leq i \leq N$). Successively higher order differences are computed until no element of the current column in the difference table is larger than the propagated error.

CALL DIFTAB (Y, N, D, ND, EPS)

INPUT: Y(I) - y_i I-th ordinate

N - no. data points

EPS - estimate of absolute errors in Y(I)

OUTPUT: D - difference table stored in packed-mode: i.e., the first-order differences are in D(1) ... D(N-1), the second-order differences in D(N) ... D(2N-2), etc.

ND - set to highest-order difference calculated.

DIFTAB

05/31/72-01153120 (,0)

DIFTAB

```
1.      SUBROUTINE DIFTAB(Y,N,D,ND,EPS)
2.      C      CALCULATES DIFFERENCE TABLE OF Y(1) ... Y(N)
3.      C      NOTE = D MUST BE DIMENSIONED AT LEAST ND*(N-1)
4.      C      ND = UPON ENTRY, MAX ORDER DIFFERENCE TO BE CALCULATED, UPON
5.      C      RETURN IS ACTUAL HIGHEST ORDER
6.      C      EPS = ABSOLUTE ERROR ESTIMATE OF Y'S TO STOP DIFFERENCES
7.      DIMENSION Y(1),D(1)
8.      MAXD = ND
9.      ERRLVL = 2.*EPS
10.     M = N
11.     T = FORDIF (Y,M,D)
12.     ND = 1
13.     K = 1
14.     100  IF (ND .GE. MAXD .OR. M .LE. 1 .OR. T .LE. ERRLVL) GO TO 200
15.     ND = ND + 1
16.     ERRLVL = 2.*ERRLVL
17.     J = K + M
18.     T = FORDIF(D(K),M,D(J))
19.     K = J
20.     GO TO 100
21.     200  RETURN
22.     END
```

ND OF COMPILATION:

NO DIAGNOSTICS.

G. FORDIF

Function which calculates the vector of forward-differences corresponding to a vector of ordinates.

CALL: DMAX = FORDIF (Y, N, D)

INPUT: Y(I) - I-th ordinate

N - No. of data

OUTPUT: D(I) - I-th forward difference, $Y(I+1) - Y(I)$

FORDIF - $\max |D(I)|, 1 \leq I \leq N-1$

FORDIF

#05/31/72#01:53:21 (-,0)

FORDIF

```
1.      FUNCTION FORDIF (Y,N,D)
2.      C      CALCULATES FORWARD DIFFERENCES D(I) = Y(I+1) - Y(I)
3.      C      RETURNS VALUE OF MAXIMUM DIFFERENCE
4.      DIMENSION Y(1),D(1)
5.      N = N + 1
6.      T = 0.
7.      DO 100 I = 1,N
8.      D(I) = Y(I+1) - Y(I)
9.      100  IF (T .LT. ABS(D(I)) ) T = ABS(D(I))
10.     FORDIF = T
11.     RETURN
12.     END
```

ND OF COMPILATION: NO DIAGNOSTICS.

H. EPSALG

Subroutine which extrapolates a sequence of partial sums to a limit by means of the ϵ -algorithm*. Only the diagonal of the matrix of con-

- - - - -

* See P. Wynn, "Five Lectures on the Numerical Application of Continued Fractions", Orientation Lecture Series No. 5, Mathematics Research Center, University of Wisconsin, Madison, Wisconsin, 53706.

- - - - -

vergent is stored.

The algorithm is as follows to find the limit of a sequence of partial sums S_m ($m = 0, 1, 2, \dots$):

$$\epsilon_{-1}^{(m)} = 0 \quad (m = 1, 2, \dots)$$

$$\epsilon_0^{(m)} = S_m \quad (m = 0, 1, 2, \dots)$$

$$\epsilon_{r+1}^{(m)} = \epsilon_{r-1}^{(m+1)} + 1/(\epsilon_r^{(m+1)} - \epsilon_r^{(m)}) \quad (r = 1, 2, \dots)$$

The $\epsilon_{2r}^{(m)}$ are improved estimates of the limit.

CALL EPSALG (S, M, X)

INPUT: S - current value of partial sum

M - Number of times EPSALG has been called previously for this series

OUTPUT: M - will be replaced by M + 1

X(1) ... X(M) - will contain the ϵ -diagonal of convergents.

REMARKS: The approximations to the limit of the series will be in every other $X(I)$. The best value for the limit will be found in $X(1)$ if M is odd or $X(2)$ if M is even.

EPSALG

05/31/72-01153122 (,0)

EPSALG

```
1.      SUBROUTINE EPSALG(S,M,X)
2.      C      EXTRAPOLATES SUM OF SERIES S BY EPSILON ALGORITHM
3.      C      S IS VALUE OF CURRENT PARTIAL SUM, AT EXIT M IS LENGTH OF
4.      C      THE EPSILON DIAGONAL X(1) ...X(M)
5.      C      BEST ESTIMATE OF SUM IS IN X(J), WHERE J = 2*MOD(M,2)
6.      DIMENSION X(1)
7.      K = M
8.      M = M + 1
9.      X(M) = 0.
10.     A1 = S
11.     100  IF (K .LE. 0) GO TO 200
12.     A0 = X(K+1) + 1./ (A1-X(K))
13.     X(K+1) = A1
14.     A1 = A0
15.     K = K - 1
16.     GO TO 100
17.     200  X(1) = A1
18.     RETURN
19.     END
```

ND OF COMPILATION:

NO DIAGNOSTICS.

I. REGFAL

This subroutine finds a root of the equation $F(x) = 0$, given an interval which contains the root, by a strategy using regula falsi and the method of bisection. Barring multiple roots or excessive rounding-error, the routine guarantees convergence. The algorithm proceeds as follows:

(1) Bisect the original interval until a sign change is found.
(If none is found, error return.)

(2) Apply regula falsi (secant method) until convergence is attained.

(a) If the change in interval length at any step is less than 10% of the previous interval length, apply the method of bisection once.

(b) If convergence is not attained, or the root is lost, error return.

CALL REGFAL (XL, XU, X, F, EPS, LIM1, LIM2, IER)

INPUT: XL, XU - Endpoints of an interval containing the root

F - name of function which stores the value of $F(x)$ in y in the call $Y = F(X)$

EPS - relative error criterion for root. Termination occurs when relative change in root is less than EPS or the root itself is less than EPS

LIM1 - Limit on number of applications of bisection to find a sign change; if LIM1 = 0, Step (1) above is skipped

LIM2 - limit on number of applications of regula falsi in step (2)

OUTPUT: X - estimate of root

IER - 0 Normal

- 1 No root or a multiple root in interval (to tolerance EPS)
- 2 No sign change found with LIM1 iterations
- 3 No convergence to EPS tolerance with LIM2 iterations
- 4 Root was lost in regula falsi iterations (no longer a sign change)

REMARK: The convergence testing could be improved slightly by adding

line 12.5 $HO = EPS * H$

and replacing line 50 with

IF (ABS(DEIX) . LT . HO) GO TO 1000

REGFAL

05/31/72-01:53:24 (,0)

REGFAL

```

1.      SUBROUTINE REGFAL (XL,XU,X,F,EPS,LIM1,LIM2,IER)
2.      C      FINDS ROOT OF THE EQTN F(X) = 0 IN INTERVAL (XL,XU)
3.      C      BY METHOD OF REGULA FALSI (GUARANTEED CONVERGENCE)
4.      C      EPS = RELATIVE ERROR TOLERANCE FOR ROOT
5.      C      LIM1 = ALLOWABLE ITER. TO FIND SIGN CHANGE IN AN INTERVAL
6.      C      LIM2 = ALLOWABLE ITERATIONS TO FIND ROOT
7.      C      IER = 0,NORMAL. = 1 NO OR MULT ROOT TO TOLERANCE EPS. = 2 NO
8.      C      SIGN CHANGE WITH LIM1 ITERATIONS. = 3 NO CONVERGENCE WITH LIM2 IT.
9.      C      = 4, LOST ROOT IN REG. FALSI ITERATIONS
10.     FA = F(XL)
11.     X = XL
12.     H = XU - XL
13.     IF (LIM1 .EQ. 0) GO TO 300
14.     J = 1
15.     HH = EPS*H
16.     DO 200 I = 1,LIM1
17.     IF (H .LE. HH) GO TO 250
18.     X = XL
19.     DO 100 K = 1,J
20.     FB = F(X+H)
21.     IF (FA*FB .LE. 0.) GO TO 350
22.     100 X = X + H
23.     H = 0.5*H
24.     200 J = 2*J
25.     IER = 2
26.     RETURN
27.     250 IER = 1
28.     RETURN
29.     300 FB = F(X+H)
30.     350 A = X
31.     B = X + H
32.     FA = F(A)
33.     HH = ABS(H)
34.     XP = A
35.     DO 800 I = 1,LIM2
36.     X = A - FA*H/(FB-FA)
37.     J = 1
38.     400 FX = F(X)
39.     IF (FX*FA ) 500,1000,600
40.     500 FB = FX
41.     B = X
42.     GO TO 700
43.     600 FA = FX
44.     A = X
45.     IF (FA*FB .GT. 0.) GO TO 900
46.     700 H = B - A
47.     IF (J .EQ. 2) GO TO 800
48.     DELX = X - XP
49.     XP = X
50.     IF (ABS(DELX) .LT. EPS*ABS(X) .OR. ABS(X) .LT. EPS) GO TO 1000
51.     IF (ABS(H) .LT. 0.9*HH) GO TO 800
52.     X = 0.5*(A+B)
53.     J = 2
54.     GO TO 400
55.     800 HH = ABS(H)

```


56. IER = 3
57. RETURN
58. 900 IER = 4
59. RETURN
60. 1000 IER = 0
61. RETURN
62. END

NO OF COMPILATION:

NO DIAGNOSTICS.

J. ADSIMP

This function returns the value of the integral

$$\int_{XL}^{XU} F(X) dX$$

obtained by means of adaptive application of Simpson's rule. The program is a slightly modified version of Alg. 182, Comm. ACM 6, 315 (1963).

CALL: VALUE = ADSIMP (XL, XU, F, ERRTOL, MAX, IER)

INPUT: XL, XU - Endpoints of the interval of integration

F - name of function which stores the value of the integrand in Y
from the call Y = F(X)

ERRTOL - Error bound on absolute error of the integral

MAX - maximum number of integration points which may be used

OUTPUT: IER - if 0, normal convergence. If $\neq 0$, then more than MAX
points are needed for convergence.

ADSIMP - Returned value of integral

REMARK: All of the dimensions in lines 6-8 could be safely reduced to
15. (which necessitates a 15 in line 41)

ADSIMP

```

05/31/72-01153:28 (,0) ADSIMP
1. FUNCTION ADSIMP(XL,XU,F,ERRTOL,MAX,IER)
2. C INTEGRATES F(X) FROM XL TO XU BY ADAPTIVE SIMPSON'S RULE
3. C ERRTOL = ALLOWABLE ABSOLUTE ERROR TOLERANCE
4. C MAX = LIMIT ON NO FUNCTION CALLS
5. C IF IER .NE. 0 MORE THAN MAX POINTS ARE REQUIRED
6. DIMENSION DX(30),EPSP(30),X2(30),X3(30),F2(30),F3(30),F4(30)
7. FMP(30),FBP(30),EST2(30),EST3(30),PVAL(30,3)
8. INTEGER RTRN(30)
9. EPS = ERRTOL
10. A = XL
11. B = XU
12. LVL = 0
13. EST = 1.0
14. DA = B - A
15. FA = F(A)
16. FM = 4.0 * F((A+B)*0.5)
17. FB = F(B)
18. KOUNT = 3
19. 100 LVL = LVL + 1
20. DX(LVL) = 0.3333333333 * DA
21. SX = DX(LVL) * 0.166666667
22. F1 = 4.0 * F(A + 0.5 * DX(LVL))
23. X2(LVL) = A + DX(LVL)
24. F2(LVL) = F(X2(LVL))
25. X3(LVL) = X2(LVL) + DX(LVL)
26. F3(LVL) = F(X3(LVL))
27. EPSP(LVL) = EPS
28. F4(LVL) = 4.0 * F(X3(LVL) + 0.5 * DX(LVL))
29. FMP(LVL) = FM
30. EST1 = SX * (FA + F1 + F2(LVL))
31. FBP(LVL) = FB
32. EST2(LVL) = SX * (F2(LVL) + F3(LVL) + FM)
33. EST3(LVL) = SX * (F3(LVL) + F4(LVL) + FB)
34. SUM = EST1 + EST2(LVL) + EST3(LVL)
35. KOUNT = KOUNT + 4
36. IF (ABS(EST-SUM) .GT. EPSP(LVL)) GO TO 500
37. 400 LVL = LVL + 1
38. I = RTRN(LVL)
39. PVAL(LVL,I) = SUM
40. GO TO (600,700,800),I
41. 500 IF (LVL .GE. 30 .OR. KOUNT .GE. MAX) GO TO 400
42. RTRN(LVL) = I
43. FM = F1
44. FB = F2(LVL)
45. EST = EST1
46. 550 DA = DX(LVL)
47. EPS = 0.577 * EPSP(LVL)
48. GO TO 100
49. 600 RTRN(LVL) = 2
50. FA = F2(LVL)
51. FM = FMP(LVL)
52. FB = F3(LVL)
53. EST = EST2(LVL)
54. A = X2(LVL)
55. GO TO 550

```

```

56.      700      RTRN (LVL) = 3
57.      FA = F3(LVL)
58.      FM = F4(LVL)
59.      FB = FBP(LVL)
60.      EST = EST3(LVL)
61.      A = X3(LVL)
62.      GO TO 550
63.      800      SUM = PVAL(LVL,1) + PVAL(LVL,2) + PVAL(LVL,3)
64.      IF (LVL .GT. 1) GO TO 400
65.      ADSIMP = SUM
66.      IER = 0
67.      IF (KOUNT .GT. MAX) IER = 1
68.      RETURN
69.      END

```

ID OF COMPILATION: NO DIAGNOSTICS.

K. SAMPLE OUTPUT

The problem shown is for the Na-Hg system with the pointwise potential taken from U. Buck and H. Pauly, J. Chem. Phys. 54, 1929 (1971).

The units of energy and length were $\epsilon = 8.79$ cpe and $r_m = 4.72 \text{ \AA}^0$, resp. The output shown is for $E^* = 1.65$.

NOTES: (1) The last partial wave calculated was at $\ell = 455$, ($b^* = 3$), when $\delta Q < 0.1 \text{ \AA}^2/b$.

(2) The convergents of the ϵ -algorithm after 5 extrapolations were:
= 175.4996 (best), 175.4999, 175.0902.

(3) The calculation took 6 seconds on an Univac 1108 (1.5 μ s add time).

Since every seventh η_ℓ was calculated, without interpolation the execution would have taken 40 seconds.

(4) The ϵ -algorithm extrapolated cross section was 696.6 \AA^2 , with $C_6^{\text{app}} = 0.6690 \times 10^5 \text{ cpe} - \text{\AA}^6$.

ENTRY TO JWKB/DNTERP

TOLERANCE FOR YO (RELATIVE) .10000-04

TOLERANCE FOR ETA (ABS) .50000-02

TOLERANCE FOR JB LIMIT .10000-01

BUCK=PAULY NA=HG 45=POINT INTERPOLATED POTENTIAL

PHASE SHIFTS AND CROSS SECTIONS FOR REDUCED MASS .342513+02

LONG-RANGE C6 .500000+00

ZERO OF POTENTIAL .810840+00

UNITS OF ENERGY AND LENGTH .879000+01 .472000+01

ENERGY 1.65000 WAVE NO. .298886+02 A=WAVE*RUNIT .141074+03

FOLLOWING TABLE IN REDUCED UNITS EUNIT,RUNIT

L	B	YO	RO	ETA	ETAJB	DELQ	IER	ISW
0	.003544	1.422920	.702780	-.856023+02	.225136+14	.175033+02	0	0
7	.053163	1.421865	.703302	-.749108+02	.296475+08	.116608+01	0	0
14	.102783	1.418988	.704728	-.647499+02	.109763+07	.908811+01	0	0
21	.152402	1.414354	.707037	-.551184+02	.153145+06	.149412+00	0	0
28	.202021	1.408074	.710190	-.460106+02	.374171+05	.162609+00	0	0
35	.251640	1.400376	.714094	-.374170+02	.124782+05	.195012+01	0	0
42	.301260	1.391112	.718849	-.293494+02	.507399+04	.233086+00	0	0
49	.350879	1.380208	.724528	-.217882+02	.236738+04	.142485+01	0	0
56	.400498	1.368192	.730892	-.147260+02	.122195+04	.276974+00	0	0
63	.450118	1.355286	.737852	-.816297+01	.681437+03	.408493+00	0	0
70	.499737	1.341338	.745524	-.209508+01	.403969+03	.374505+00	0	0
77	.549356	1.326383	.753930	.347989+01	.251643+03	.605077+01	0	0
84	.598975	1.310477	.763081	.855836+01	.163309+03	.347806+00	0	0
91	.648595	1.293687	.772984	.131465+02	.109695+03	.194877+00	0	0
98	.698214	1.276065	.783659	.172409+02	.758775+02	.697211+00	0	0
105	.747833	1.257647	.795136	.208403+02	.538309+02	.623540+00	0	0
112	.797452	1.238331	.807538	.239393+02	.390420+02	.689164+00	0	0
119	.847072	1.218499	.820682	.265423+02	.288705+02	.825251+00	0	0
126	.896691	1.198434	.834422	.286279+02	.217191+02	.107484+00	0	0
133	.946310	1.176721	.849819	.301672+02	.165916+02	.851474+00	0	0
140	.995929	1.154330	.866303	.311727+02	.128503+02	.577642+01	0	0
147	1.045549	1.130917	.884238	.316020+02	.100771+02	.357779+01	0	0
154	1.095168	1.105848	.904284	.314321+02	.799193+01	.286874+03	0	0
161	1.144787	1.079500	.926355	.306323+02	.640371+01	.570406+00	0	0
168	1.194406	1.050014	.952368	.291102+02	.517958+01	.657322+00	0	0
175	1.244026	1.017124	.983165	.268476+02	.422580+01	.121839+01	0	0
182	1.293645	.978690	1.021774	.237233+02	.347520+01	.126025+01	0	0
189	1.343264	.929633	1.075693	.197253+02	.287904+01	.792292+00	0	0
196	1.392883	.864247	1.157077	.149959+02	.240149+01	.594686+00	0	0
203	1.442503	.790788	1.264561	.103836+02	.201591+01	.966429+00	0	0
210	1.492122	.725005	1.379301	.707472+01	.170229+01	.755222+00	0	0
217	1.541741	.684871	1.460130	.527661+01	.144543+01	.110085+01	0	0
224	1.591360	.654228	1.528519	.405952+01	.123371+01	.100412+01	0	0
231	1.640980	.628806	1.590316	.313450+01	.105813+01	.826042+04	0	0
238	1.690599	.604714	1.653675	.237284+01	.911701+00	.817165+00	0	0
245	1.740218	.584066	1.712136	.185593+01	.788927+00	.160253+01	0	0
252	1.789837	.565683	1.767773	.147790+01	.685468+00	.177444+01	0	0
259	1.839457	.548497	1.823165	.117491+01	.597871+00	.156592+01	0	0

266	1.889076	.533001	1.876168	.991833+00	.523369+00	.132352+01	0	0
273	1.938695	.518827	1.927424	.855278+00	.459735+00	.110438+01	0	0
280	1.988314	.505414	1.978574	.734174+00	.405163+00	.892486+00	0	0
287	2.037934	.492703	2.029621	.632512+00	.358183+00	.712228+00	0	0
294	2.087553	.480683	2.080371	.548260+00	.317591+00	.567089+00	0	0
301	2.137172	.469277	2.130939	.477267+00	.282395+00	.450956+00	0	0
308	2.186791	.458430	2.181358	.417145+00	.251778+00	.358958+00	0	0
315	2.236411	.448098	2.231656	.365977+00	.225059+00	.286406+00	0	0
322	2.286030	.438240	2.281854	.322221+00	.201672+00	.229249+00	0	0
329	2.335649	.428822	2.331968	.284637+00	.181141+00	.184175+00	0	0
336	2.385268	.419813	2.382014	.252239+00	.163068+00	.148570+00	0	0
343	2.434888	.411184	2.432001	.224201+00	.147116+00	.120355+00	0	0
350	2.484507	.402911	2.481939	.199832+00	.133001+00	.978999-01	0	0
357	2.534126	.394970	2.531835	.178604+00	.120480+00	.799813-01	0	0
364	2.583745	.387342	2.581696	.160043+00	.109347+00	.656165-01	0	0
371	2.633365	.380008	2.631527	.143761+00	.994260-01	.540507-01	0	0
378	2.682984	.372949	2.681332	.129441+00	.905659-01	.447026-01	0	0
385	2.732603	.366151	2.731115	.116801+00	.826366-01	.371101-01	0	0
392	2.782222	.359599	2.780879	.105632+00	.755259-01	.309289-01	0	0
399	2.831842	.353279	2.830626	.957176-01	.691369-01	.258658-01	0	0
406	2.881461	.347179	2.880358	.869143-01	.633857-01	.217121-01	0	0
413	2.931080	.341288	2.930078	.790664-01	.581991-01	.182855-01	0	0
420	2.980699	.335594	2.979788	.720631-01	.535136-01	.154523-01	0	0
427	3.030319	.330089	3.029487	.657892-01	.492735-01	.130970-01	0	0
434	3.079938	.324762	3.079179	.601676-01	.454303-01	.111364-01	0	0
441	3.129557	.319605	3.128863	.551144-01	.419412-01	.949672-02	0	0
448	3.179176	.314610	3.178540	.505678-01	.387688-01	.812256-02	0	0
455	3.228796	.309769	3.228217	.464612-01	.358800-01	.696481-02	0	0

MAINING CROSS SECTION IS LESS THAN 0.05 SQ ANG

SILON ALGORITHM CONVERGES ...

175.4996 =54.9791 175.4999 102.8419 175.0902

ME (SEC) 5.937

CROSS SECTION AT LAST PHASE SHIFT 694.92 Q 175.090

JB EXTRAPOLATED CROSS SECTION (SQ ANG) 696.51 QJB 175.490 C6 APPARENT .668939

HIGHEST ORDER DIFFERENCE USED IN INTERPOLATION 10

EPSILON ALGORITHM CROSS SECTION 696.55 Q 175.500 C6 APPARENT .669031+05